#### TABLE 1-1. Model M-100 General Performance Specifications

#### OUTPUT CHARACTERISTICS

Frequency: 10 MHz Sine Wave,  $(\pm 5 \times 10^{-11})$  at shipment)

Amplitude: 0.5 vrms (-10% + 30%) into 50 ohm load

Phase Noise (SSB 1 Hz BW): > 120 dB at 100 Hz from carrier

(Signal-to-Noise) > 130 dB at 1000 Hz from carrier

Harmonic Distortion: > -30 dBc Non-Harmonic Distortion: > -80 dBc

Warm-up: < 10 minutes to reach 10 MHz  $\pm 2 \times 10^{-10}$  at 25°C ambient < 30 minutes to reach 10 MHz  $\pm 5 \times 10^{-11}$  at 25°C ambient

Peak current during warm-up: approx. 2.2 amps max. at 25°C with 26 vdc input.

#### INPUT

Voltage: 22.5 to 32.0 Vdc (50 V, 50 ms transient).

Power: 18 watts max. at 25°C with 26 vdc input.

 $<1 \times 10^{-11}$  for  $\pm$  10 % input voltage change.

#### STABILITY

Long-Term Drift:  $\leq 6 \times 10^{-11}$  for the first month after 14 days of continuous operation.  $\leq 3.6 \times 10^{-10}$  for the first year, total period;  $\leq 2 \times 10^{-10}$  for the second year.

Short-Term Stability:  $\sigma y(\tau) = 3 \times 10^{-11} \times (\tau^{-\frac{1}{2}})$  for 1 sec  $\langle \tau \langle 100 \text{ seconds} \rangle$ Magnetic Field:  $\langle 3 \times 10^{-13}/\text{AM}^{-1} \rangle$  worst case orientation (2.4 x  $10^{-11}/\text{Gauss}$ )

#### GENERAL

Frequency Trim Range Adjustment: > 3 x 10<sup>-9</sup>

Settability:  $1 \times 10^{-11}$ Retrace:  $\pm 1 \times 10^{-11}$ 

Operating Temperature: < 3 x 10<sup>-10</sup> from -55°C to +68°C

(-67°F to 155°F) at baseplate

Storage Temperature (non-operational): -62°C to +85°C (-80°F to 185°F)

Size (inches): 4.81 high x 3.90 wide x 3.94 deep (see Outline Dwg No. 70549-1)

Weight: 4.0 1b max. without heat sink

4.5 1b max. with standard heat sink attached.

1-7 EXTERNAL ADJUSTMENT POINTS AND CONNECTIONS. Figure 1-1 illustrates the front and rear views of the M-100. Table 1-2 details all externally accessible connections and adjustments.

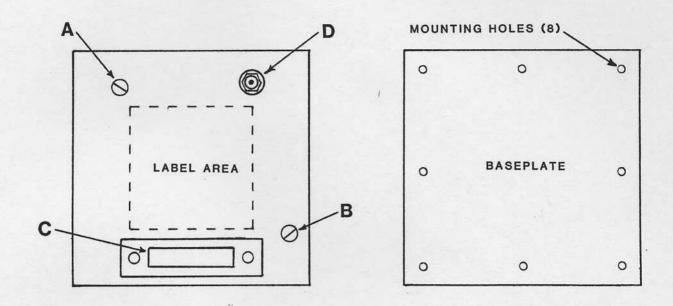


Figure 1-1. M-100 Front and Rear Views

Table 1-2

A	Crystal Trim Adjustment (Refer to Section 5-13 for adjustment procedure)		
В	Frequency Adjustment (Refer to Section 3-4.7 for adjustment procedure)		
С	J2 Connector M28748/7-D00FlA (mates with M28748-18-D10LIA)  Pin B = Rb Lamp Voltage Signal Pin F = Xtal Control Voltage Signal Pin H = Resonance Lock Signal Pin L = +22.5 to +32 Vdc Input Pin P = Ground		
D	J1 Connector - 10 MHz Output Type SMA, MIL-C-39012		

## CHAPTER 2

#### CAUTION

THE UNIT'S OUTER COVER IS A SPECIALLY DESIGNED MAGNETIC SHIELD; DAMAGE TO THE OUTER COVER COULD CHANGE ITS SHIELDING CHARACTERISTICS.

- 2-1 RECEIVING AND INSPECTION. The M-100 is packaged and shipped in a foampacked container. The unit is inspected mechanically and electrically
  prior to shipment. If the shipping carton is damaged, ask that the
  carrier's agent be present when the unit is unpacked. The unit should be
  inspected for external damage (i.e. scratches, dents, or broken connectors). If damage is discovered, or if the unit fails the Operational
  tests, notify the carrier, and Ball Corporation, Efratom Division,
  3 Parker, Irvine, CA 92718-1605. Telephone (714) 770-5000; Telex 685-635.
  In Europe: Efratom Elektronik GmbH, Am Perlacher Forst 186, D-8000,
  Munchen 90, West Germany. Telephone (089) 648059. Retain the shipping
  carton and the foam-packing material for the carrier's inspection.
- 2-2 SHIPPING. If reshipment of the unit is necessary, the original container and packing should be used. If the original container is not available, a suitable container with foam-packing is recommended.
- 2-3 STORAGE. Temperatures during storage should be limited as follows:
  - (a) maximum temperature: +85°C (185°F)
  - (b) minimum temperature: -62°C (-79°F)
- 2.4 MOUNTING. The unit's mounting plate has been drilled and tapped to accommodate installation. Although the unit is shipped ready for installation, sufficient airflow must be provided to ensure that the unit's baseplate temperature does not exceed 68°C (154°F) during operation. The unit may be mounted with the aluminum thermal baseplate in contact with a flat\* metal surface.

The heat transfer characteristics of the mounting surface must be adequate to limit the rise of the unit's baseplate to +68°C. The allowable environmental temperature (Ta) for this mounting is:

$$Ta = +68^{\circ}C - (V_{s} \times I_{s} \times R_{k})$$

Where: V = Supply Voltage in volts.

I = Supply Current in amperes.

 $R_k$  = Thermal Resistance between unit and ambient, (°C/watt).

2-5 POWER REQUIREMENTS. The M-100 requires an external power source capable of providing between +22.5 vdc and +32 vdc, with a minimum output of 2.0 amp. The positive input voltage is to J2 pin L, the negative return voltage on J2 pin P.

In order to obtain the cleanest output signal close to the carrier, the maximum ac ripple on the supply voltage must be less than 100 mV peak-to-peak. If it is acceptable for the output frequency to contain spurious multiples of the powerline frequency (50, 60, or 400 Hz), the ripple can be higher, but in no case should the supply voltage AC +/- peak exceed the upper or lower input power limit of the unit.

- 2-6 MONITORING SIGNAL OUTPUTS. Figure 2-1 illustrates the pin connections for the J2 connector and presents a brief functional description of the connections.
  - J2 B. Rb LAMP VOLTAGE SIGNAL
    - F. XTAL CONT VOLTAGE SIGNAL
    - H. RESONANCE LOCK SIGNAL
    - L. +22.5 to +32 Vdc Input
    - P. GROUND

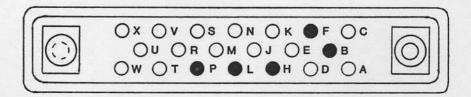


FIGURE 2-1. J2 Connector and Pin Arrangement.

2-7 INSTALLATION CONSIDERATIONS. Some consideration must be given to the operating location of the unit, regardless of its application. To minimize frequency offsets and/or non-harmonic distortion, the unit should not be installed near equipment generating strong magnetic fields such as generators, transformers, etc.

#### CAUTION

Care must be taken to ensure that the maximum operating temperature is not exceeded (+68°C as measured at the unit's baseplate).

# CHAPTER 3 OPERATION AND FUNCTIONAL TESTS

3-1 TEST EQUIPMENT. The test equipment required to perform operational and functional tests is listed in Table 3-1. Test equipment other than those items listed may be used, provided that the performance equals or exceeds the MINIMUM USE CHARACTERISTICS as stated in Table 3-1.

TABLE 3-1. Functional Operation Test Equipment

Item	Minimum Use Characteristics	Test Equipment
3.1 DC Power	Output Voltage: 0 to 30 Vdc	Hewlett-Packard
Supply	Output Current: 3.0 Amp	6296A or 6433B
3.2 Digital	Voltage Range: 0 to 30 Vdc	Fluke 8000A or
Multimeter	Accuracy: <u>+</u> 1.25%	8020A
(DMM)	Resistance Range: 0 to 150 ohm	
3.3 Atomic	Internal Ref Frequency: 10 MHz	Efratom TS-105A
Oscillator	Accuracy: <u>+</u> 1x10 <sup>-11</sup>	or TS-105
Test Set	Stability: parts in 10 <sup>12</sup>	
3.4 Resistive Load	Feed-thru type, 50 ohm	Hewlett-Packard 10100C or Pomona Electric 4119-50
3.5 Timer	Capable of indicating 1 min to 15 min	Any wristwatch or wall clock
3.6 Optional External Frequency Ref.	Output Frequency: 10 MHz Accuracy: $\pm$ 5 x $10^{-12}$ Stability: Parts in $10^{12}$ or as required by application	1. Efratom RGR 2. Cesium Standard 3. Efratom Hydrogen Maser 4. Efratom MVLF
3.7 Adapter	SMA Male to BNC Female	Pomona Electric Model 4119-50

3-2 NORMAL OPERATION. With the output connector J1 terminated with a 50-ohm resistive load, and the required input power applied to the pins L (+) & P (-) of connector J2, the unit will immediately begin producing a 10-MHz signal from the crystal oscillator. Within approximately 10 minutes after application of input power, the unit will "lock". At that time the crystal is stabilized by the atomic resonant frequency.

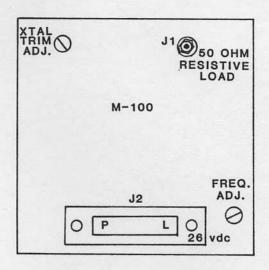


Figure 3-1. Connections for Normal Operation NOTE

Throughout the test procedures, the Model M-100 may be referred to as the UUT (Unit Under Test). Also, all connections described or illustrated are for the standard configuration, SMA-type coaxial connector J1, and standard connector J2; if the UUT has a different connector arrangement, make the described connections to the appropriate pins as described in the pin diagram accompanying the UUT.

- 3-3 ATOMIC RESONANCE LOCK, AND VCXO CONTROL VOLTAGE TESTS.
- 3-3.1 Connect equipment as shown in Figure 3-2 with the 50-ohm feedthrough connected at the M-100 output connector J1. Do not make the dotted-line connection until instructed to do so.

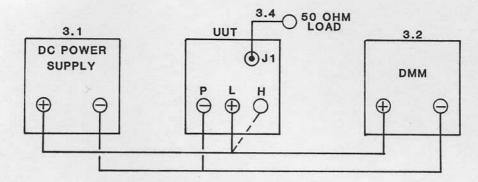


Figure 3-2 Test Setup for Atomic Resonance Lock Test

- 3-3.2 Adjust the dc power supply controls to obtain a  $26 \pm 1.3$  Vdc indication on the DMM. Note the time (item 3.5) input power is applied to the unit.
- 3-3.3 Disconnect the DMM positive lead connected to J2 pin L without disturbing the positive input voltage connection.
- 3-3.4 Set the DMM to measure resistance in the 200-ohm range. (Do not use the Auto Range for this test.)
- 3-3.5 Connect the DMM positive lead to J2 pin H (Figure 3-2 dotted-line connection). Monitor the DMM indication during warm-up.

#### NOTE

During warm-up the DMM will indicate overrange. Within 10 minutes after power application, the DMM should indicate approximately 150-ohm, indicating that the crystal oscillator has become locked to the atomic reference frequency.

- 3-3.6 Verify that atomic lock occurs  $\leq$  10 minutes after application of input power to the M-100.
- 3-3.7 After the atomic lock has been verified, remove the DMM positive lead from J2 pin H, and set the DMM controls to measure dc voltage in the 20 volt range.
- 3-3.8 Connect the DMM positive lead to J2 pin F, and verify that the DMM indication is between +2 and +15 vdc.

#### NOTE

If the DMM indication is not between +3 and +17 vdc refer to Chapter 5, Maintenance, for the adjustment procedure.

- 3-4 OPERATIONAL FREQUENCY ACCURACY TEST
- 3-4.1 Connect the equipment as shown in Figure 3-3.

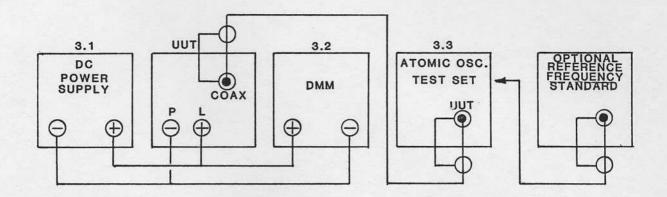


Figure 3-3 Operational Frequency Accuracy Test Setup.

- 3-4.2 Adjust the dc power supply controls to obtain a  $26 \pm 1.3$  vdc indication on the DMM.
- 3-4.3 Allow sufficient time for equipment to stabilize.

#### NOTE

The UUT requires 10 minutes stabilization to obtain the following frequency accuracy:  $\pm 2 \times 10^{-10}$  of the final frequency (calibrated frequency), or the frequency before the unit was turned off (if turnoff was within 24 hours). If the UUT was in storage, the worse-case error =  $\pm 2 \times 10^{-10}$  warm-up +/- last calibration accuracy, or  $5 \times 10^{-11}$  factory setting at shipment (whichever is applicable) + \*aging specification.

The UUT requires 1 hour stabilization time to obtain the following accuracy:  $\pm 2 \times 10^{-11}$  of final frequency or frequency at turnoff (if turnoff was within 24 hours). If UUT was in storage, the worse case error =  $\pm 2 \times 10^{-11}$  warm-up +/-last calibration accuracy, or  $5 \times 10^{-11}$  factory setting at shipment, whichever is applicable  $\pm$  aging specification.

<sup>\*</sup> Aging Specification: (refer to the Table 1-1, Specifications).

- 3-4.4 If necessary, press the test set's ADVANCE switch to unblank the display, then press the RESET switch to obtain the READY message.
- 3-4.5 Perform all necessary menu option selections and bring the READY message back to the display. Ensure that "UUT 10 MHz" is part of the bottom-line message.
- 3-4.6 Press the test set's RESET push button to begin the test. Allow the test set sufficient time to obtain the UUT's FREQ OFFSET indication for the 100 sec AVR TIME, and the UUT's ALLAN VARIANCE indication for at least the 10 sec AVR TIME, (the 100 sec freq offset will have to update 10 times in order to obtain the 10 sec Allan Variance test results).
- 3-4.7 Allow sufficient time for the test set to indicate the UUT OFFSET for the data you require. Verify that the UUT frequency offset is within the tolerance stated in the NOTE following Step 3-4.3.

#### NOTE

If the UUT is not within the stated tolerance limits continue with the Frequency Adjustment procedure, paragraph 3-4.7.1 and 3-4.7.2.

3-4.7.1 Refer to Figure 3-4 to locate the M-100 frequency adjustment screw access hole.

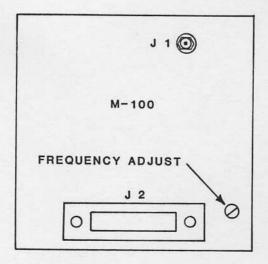


Figure 3-4 Location of M-100 Frequency Adjustment

3-4.7.2 Using the appropriate alignment tool and monitoring the test set indication, rotate the 20-turn potentiometer (adjustment screw) clockwise (frequency increase) or counterclockwise (frequency decrease) as necessary, until the test set display indicates the M-100 is within the required tolerence (or  $\pm$  5x10<sup>-11</sup>) for the three averaging times.

NOTE

If the unit has aged beyond the adjustment capability of the frequency adjust potentiometer, refer to the Maintenance chapter for appropriate procedures.

3-5 SHORT-TERM STABILITY TEST (ALLAN VARIANCE)

NOTE

If you have just completed 3-4 through 3-4.7, the Allan Variance (AV) indications on the test set are valid. If 3-4 was not performed, continue with 3-5.1.

- 3-5.1 Connect the equipment as illustrated in Figure 3-3.
- 3-5.2 Adjust the dc power supply controls to obtain a 26  $\pm$  1.3 Vdc indication on the DMM.
- 3-5.3 Allow sufficient time for equipment to stabilize.
- 3-5.4 If necessary, press the test set's ADVANCE switch to unblank the display, then press the RESET switch to obtain the READY message.
- 3-5.5 Perform all necessary menu option selections and bring the READY message back to the display. Ensure that "UUT 10 MHz" is part of the bottom-line message.
- 3-5.6 Press the test set's RESET push button to begin the test. Allow the test set sufficient time to obtain the UUT's AV indication for at least the 10 sec AVR TIME. (The 100 sec FREQ OFFSET will have to update 10 times in order to obtain the 10 sec AV test results.)
- 3-5.7 Allow sufficient time for the test set to indicate the UUT AV, as required. Verify that the UUT AV is within the tolerance limits for short-term stability, as stated in Table 1-1.

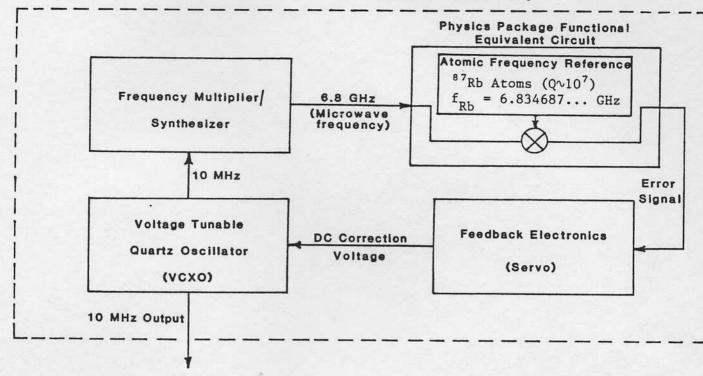
## CHAPTER 4 THEORY OF OPERATION

- 4-1 INTRODUCTION. This chapter of the manual contains a general theory of operation and circuit description of the Model M-100 rubidium frequency Standard. Schematic diagrams and parts lists are included in the Appendix.
- 4-2 GENERAL THEORY OF OPERATION. The M-100 generates a frequency-stable 10 MHz output signal from a Voltage-Controlled-Crystal-Oscillator (VCXO) which is locked to an atomic frequency reference. The atomic frequency reference is the 6.834 GHz ground-state hyperfine transition of <sup>87</sup>Rb (rubidium). The rubidium atoms which provide the atomic frequency reference are contained in a resonance cell within a resonator assembly. The VCXO is locked to the rubidium resonant frequency ( $f_{Rb}$ ), at approximately 6.8 GHz, in the following manner. A microwave signal near  $\boldsymbol{f}_{\mbox{\scriptsize Rb}}$  is synthesized from the  $10~\mbox{\scriptsize MHz}$ VCXO output and used to excite the rubidium atoms contained within a microwave cavity. The frequency synthesis scheme is designed so that the VCXO frequency is exactly 10 MHz when the microwave frequency is exactly equal to  $f_{ph}$ . The frequency of the signal applied to the microwave cavity can be maintained equal to f<sub>Rh</sub> by generating an error signal when the microwave frequency differs from f<sub>Rb</sub>. This error signal is fed back and adjusts the VCXO with a control voltage (Figure 4-1) maintaining its frequency at exactly 10 MHz.

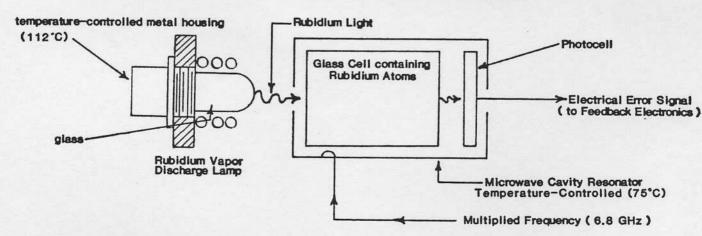
The error signal is generated by the physics package which consists of the rubidium lamp and the resonator assembly. Light from the rubidium lamp is generated by an RF-excited plasma discharge and passes into the resonator assembly where it interacts with the rubidium atoms contained in the resonance cell. Some of this light reaches the photocell inside the resonator assembly. When the applied microwave frequency is equal to  $f_{\rm Rb}$ , the rubidium atoms resonate with the microwave field in the cavity. This causes the light reaching the photocell to decrease such that the photocell

## SIMPLIFIED BLOCK DIAGRAM OF RUBIDIUM ATOMIC STANDARD

(Atomic Standards DO NOT use nuclear radioactivity)



### RUBIDIUM STANDARD PHYSICS PACKAGE



When the multiplied frequency equals the rubidium atom frequency, the error signal is zero. When the two frequencies are different, an error signal is generated that is used to "steer" the Quartz Oscillator frequency to the correct value.

Figure 4-1. Simplified Block Diagram and Physics Package

output current is a minimum at exact resonance (i.e., when the injected microwave frequency is exactly equal to  $f_{Rb}$ ; refer to Figure 4-1). An explanation of this phenomenon requires a detailed description of the physics of rubidium atoms and their simultaneous interaction with light and microwave radiation. This description is provided in section 4-2.1.2, Optical Pumping. A microwave modulation technique is used continuously to minimize the photocell current thereby locking the VCXO to  $f_{Rb}$  (Figure 4-1).

To enhance understanding of the operation of the rubidium standard, it is suggested that the reader refer frequently to the Modulation Concept (Figure 4-2), the Simplified Block Diagram (Figure 4-1), and the Detailed Block Diagram (Figure 4-5).

4-2.1 Atomic Reference Frequency/Physics Package. The physics package consists of a resonator section and a lamp section, each supported by additional circuitry. The lamp section consists of a temperature-controlled (thermostated) Rb lamp and an RF lamp exciter. The lamp exciter is frequently referred to as the lamp oscillator. To maintain a sufficient and well-defined Rb vapor pressure in the lamp envelope, the lamp thermostat is set to approximately 115°C. A high-energy (~1 W) RF-field of approximately 80 MHz is generated by the lamp exciter. This field starts and maintains an electrodeless plasma gas discharge in the lamp envelope. The lamp light contains the desired spectral lines of Rb necessary for the optical pumping process.

The resonator contains the integrated Rb cell, a photocell, a step recovery diode (with coupling loop), and the C-field windings. The density of the Rb atoms in the cell is thermostatically controlled in a manner similar to that used for the lamp.

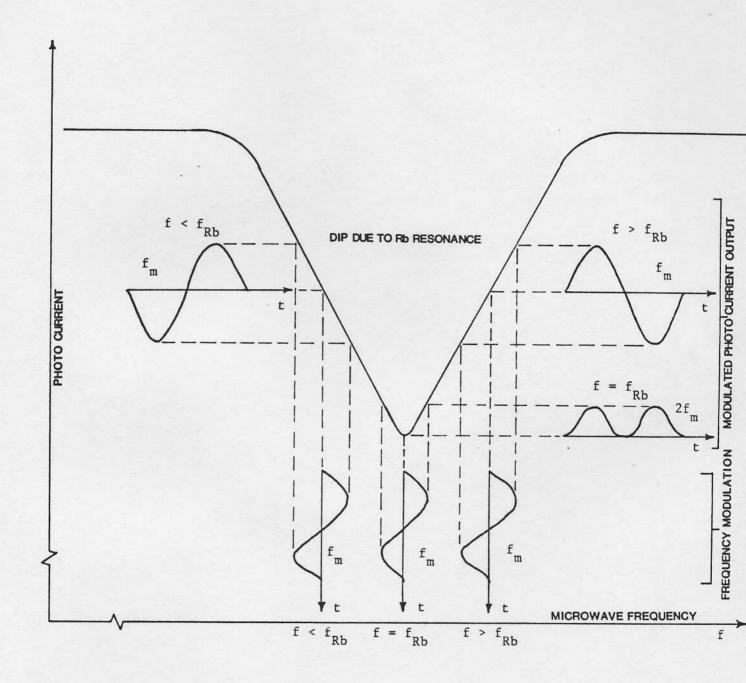


Figure 4-2. Derivation of Modulation Signal

A 60 MHz signal generated by the Multiplier printed circuit board (PCB) and a 5.3125 MHz signal from the frequency synthesizer is fed to the step recovery diode/coupling loop mounted in the resonator cavity. This circuit generates radiation having frequencies given by the expression (60n + 5.3125m) MHz, where n = a positive integer and m = an integer. The microwave frequency (f) of interest here is that for which n = 114 and m = -1:

114 x 60 MHz
- 5.3125 MHz
6 834.687 500 MHz.

The Rb resonance cell and the multiplication/synthesis technique are utilized so that the microwave frequency is exactly equal to the ground-state hyperfine frequency of  $^{87}\text{Rb}$  (fRb = 6834.687500 MHz) when the external output frequency of the M-100 is exactly 10 MHz. Adjustment of the current flowing through the C-field coil allows fine tuning (parts in  $^{9}$  and less) of the hyperfine transition frequency (via the second-order Zeeman effect) and therefore the 10 MHz output frequency.

With the correct microwave signal generated in the cavity and the proper Rb vapor pressure in the lamp and cell, the light intensity passed by the cell will be a function of the microwave frequency. Figure 4-2 illustrates this concept. The photocell output current is proportional to the intensity of the light incident upon the photocell. When the injected microwave frequency f is exactly equal to the frequency  $f_{Rb}$  of the ground-state hyperfine transition of  $^{87}{\rm Rb}$ , maximum energy is absorbed from the pumping light resulting in minimum photo current.

The "dip" in the photo-current-versus-microwave-frequency curve of Figure 4-2 is very small: on the order of 0.1% of the total photo current. For this reason, DC detection of the dip is not feasible and an AC detection method is utilized. The AC method involves frequency modulating the microwave radiation at an audio frequency  $f_m$  (= 127 Hz for the M-100). As shown in Figure 4-2, this modulation produces a corresponding modulation of the output current from the photocell. When the microwave frequency is exactly equal to the rubidium hyperfine frequency (f =  $f_{\rm Rb}$ ), the modulated

M-100

photo current contains no AC component at the modulation frequency  $f_{\rm m}$  but there is a component at twice the modulation frequency  $2f_{\rm m}$  (= 254 Hz for the M-100); the presence of this second harmonic of the modulation indicates that the VCXO is locked to the hyperfine transition. If the microwave frequency is greater than the rubidium frequency (f >  $f_{\rm Rb}$ ), then the photo current will contain an AC component at the fundamental frequency  $f_{\rm m}$  that is in phase with the original modulation at frequency  $f_{\rm m}$ . If the microwave frequency is lower than the rubidium frequency (f <  $f_{\rm Rb}$ ), then the photo current will contain an AC component at the fundamental frequency  $f_{\rm m}$  that is 180° out of phase with the original modulation at frequency  $f_{\rm m}$ .

The DC error signal that is used to correct the frequency of the VCXO is derived from the AC component of photo current at the fundamental frequency  $f_m$  by synchronous rectification (demodulation) of the latter. As can now be understood from the previous description of Figure 4-2, when the VCXO is exactly on frequency (10 MHz for the M-100) there is no AC component of photo current at the fundamental frequency  $f_{\rm m}$  of the modulation and therefore no corresponding DC error signal (in this case, there is no need to correct the VCXO frequency). Should the VCXO frequency drift upwards, the microwave frequency will also drift up and the condition f >  $f_{\mbox{\scriptsize Rb}}$  will occur. Synchronous rectification of the AC component of the photo current will, in this case, produce a positive DC error signal that is proportional to the amplitude of the fundamental component. Conversely, if the VCXO frequency drifts down instead of up, the condition f  $\langle$  f<sub>ph</sub> will occur. In this case, the synchronous rectification will produce a negative DC error signal that is proportional to the amplitude of the fundamental component of the photo current. (The sign reversal is due to the 180° phase change in the modulated photo current when  $f < f_{Rh}$ ). The phase information contained in the fundamental component of the photo current is used to steer the VCXO frequency and cancel the offset, therefore locking it to fRb.

The above modulation scheme is implemented by phase modulating (at  $f_m$ ) the 30 MHz on the multiplier PCB which, when doubled by the doubler and multiplied by 114 by the step recovery diode, produces frequency modulation (at  $f_m$ ) of the 6.8 GHz microwave signal. The resulting AC photo current is amplified and synchronously rectified on the servo PCB to provide the DC

error signal. However, instead of routing the DC error signal directly to the VCXO, it is electronically integrated and then routed to the VCXO. This then completes the description of the servo loop. This type of servo loop is commonly used in passive atomic frequency standards and is known as a "frequency-locked loop."

- 4-2.1.1 Electronic Analogue of Physics Package. The physics package of the M-100 is a passive device in the sense that the  $^{87}$ Rb atoms must be "interrogated" by externally-generated microwave radation; the atoms themselves do not produce a self-sustaining oscillation at the atomic hyperfine frequency. To a first approximation, the behavior of the  $^{87}$ Rb atoms in the resonance cell can be represented by an electrical analogue, as shown in Figure 4-3. In this analogue, the atoms behave like an ultra-stable, high Q (Q  $\sim$  10  $^{7}$ ), series-resonant RLC tank circuit that is resonant at the hyperfine frequency ( $f_{Rb} = 6.834$  ... GHz). The analogue of the microwave signal derived from the 10 MHz VCXO is a frequency-modulated voltage source operating at f = 6.8 GHz to drive the tank circuit. Similarly, the analogue of the photocell is a square-law current detector and a low-pass filter.
- 4-2.1.2 Optical Pumping. In the actual physics package, the atomic resonance is detected by optical means, specifically by a decrease in the intensity of the Rb light transmitted by the resonance cell when the frequency (f) of the interrogating microwave signal is in the vicinity of the atomic resonant frequency (f  $\sim$  f\_Rb). To understand why this effect occurs, it is necessary to consider the atomic physics phenomenon known as "Optical Pumping". In this section, an oversimplified description of the optical pumping process is given that serves to illustrate the basic principle involved in the detection of the atomic resonance. In all that follows, it is important to note that the frequency f\_O of any atomic resonance transition is related to the difference in the energies  $E_O$  of the two atomic energy levels, between which the transition occurs, by the fundamental equation of physics,

 $f_o({\rm Hz}) = E_o({\rm joules})/h,$  Where h = Planck's constant =  $6.6262 \times 10^{-34}$  joules/Hz.

## PHYSICS PACKAGE

### **ELECTRONIC ANALOGUE**

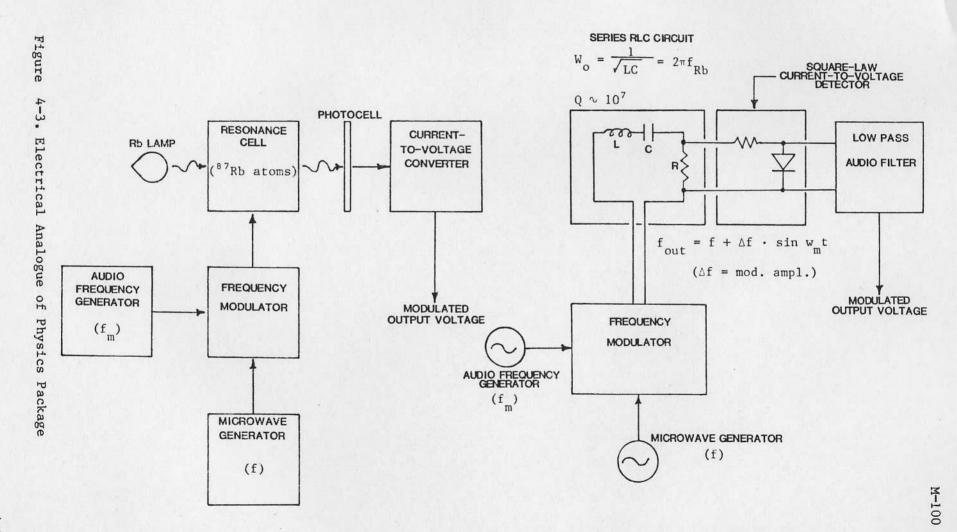


Figure 4-4 is a simplified diagram of the energy levels involved in the optical pumping process. The two lower levels, A and B, are the two ground-state hyperfine levels. In the absence of light from the rubidium lamp, the rubidium atoms in the resonance cell will be equally divided between these two levels, as indicated in frame 1 of Figure 4-4. If the atoms are irradiated with microwave energy at the hyperfine frequency, then those atoms in level A will make a transition to level B and vice-versa, without changing the number of atoms in each of the two levels (both levels still equally populated), and the transitions will not be detectable. However, if a method can be found to create a difference in the atom populations of the two states A and B, then the transition can be detected (as will be explained below). The method used to create a population difference is called "optical pumping" and in the case of the M-100 it is used to transfer (or "pump") atoms from level A to level B. As the name implies, the pumping is done indirectly by optical means and involves a third energy level of atom labelled C in Figure 4-4. (For the 87Rb atom, the energy spacing between level C and level A is approximately 55,000 times greater than the spacing between levels B and A, therefore, the diagram is not to scale.)

Level C is an optically-excited state of the atom which is normally vacant; for rubidium, this C level state is excited by infrared light energy of the proper wavelength from the rubidium lamp. Transitions to level C are known as "optical transitions" and can occur from either of the two hyperfine energy levels A or B. If only the spectral wavelength corresponding to one of the hyperfine levels is introduced (no microwave radiation is present), only the atoms in that hyperfine level will make transitions to level C. This condition can be realized by removing the spectral wavelength corresponding to the hyperfine level B using the method of optical hyperfine filtering. (In the M-100, the filtering process is carried out in the resonance cell itself using <sup>87</sup>Rb atoms.)

If the light energy injected into the resonance cell corresponds to the wavelength required for level A to C transitions, the rubidium atoms at the A level will absorb some of the light. As indicated in frame 2 of Figure 4-4, this absorption of light raises those atoms to the higher C level

energy state. After a short time ( $^{\circ}$  30 ns) the atoms which were raised to the C level will emit a photon of approximately the same wavelength as that which raised the atoms to the optically-excited state; they then return to the ground-state hyperfine level, redistributing themselves approximately equally between levels A and B (frame 3). The atoms which return to level A will again absorb the light and be raised to level C, where they will again remain for a short time before emitting photons and again redistributing themselves between the two hyperfine energy levels A and B (frame 4). By this optical pumping method, a population difference is produced between the two hyperfine levels whereby all of the atoms are pumped from level A into level B (frames 5-7). Once this idealized condition exists, there are no atoms left in level A to be excited to level C and the light is not the proper wavelength to excite the atoms in level B to level C (frame 7). Thereafter, no light attenuation occurs when the light passes through the resonance cell.

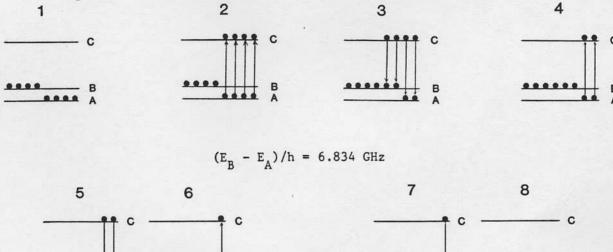
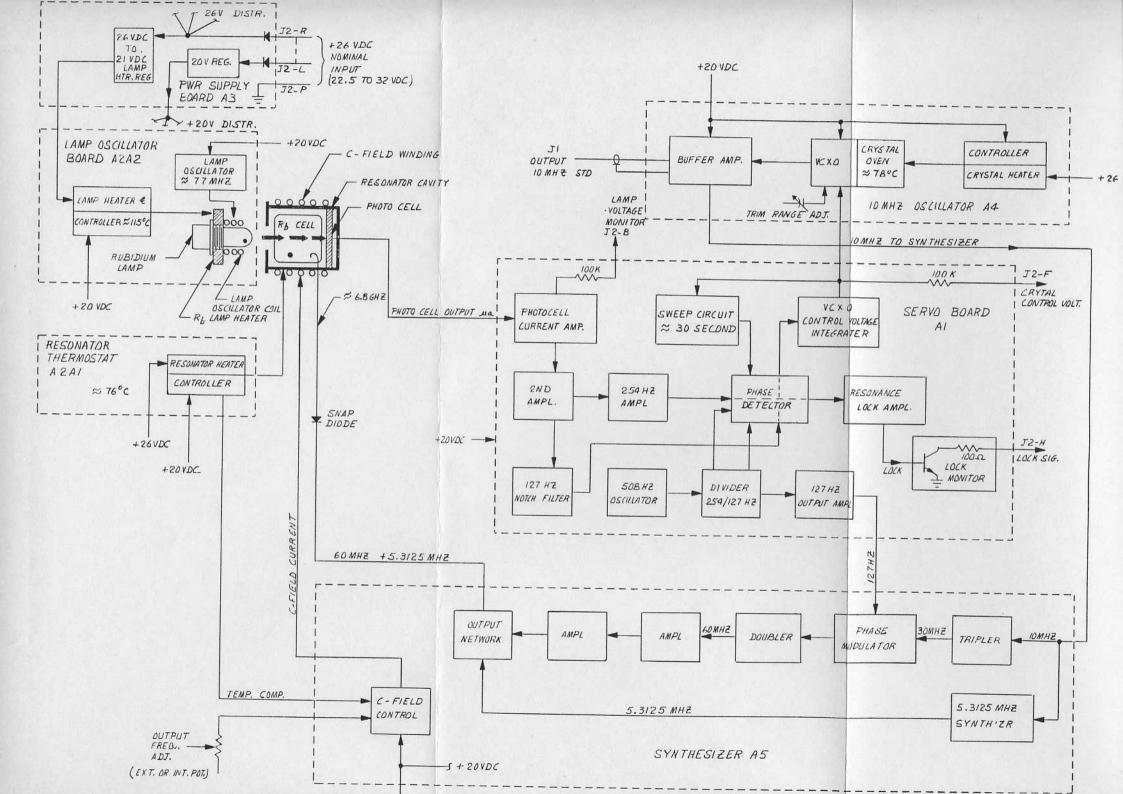


Figure 4-4. Optical Pumping Process Illustrated.

When a microwave field corresponding to the hyperfine frequency is now applied simultaneously with the pumping light, the atoms in level B make transitions to level A and are then available for excitation to level C by the light beam. Since each optical excitation of an atom from level A to level C requires the absorption of a light photon, the net effect of applying the microwave field is to cause attenuation of the light beam with the attentuation being greatest when the frequency, f, of the microwave field is exactly equal to the hyperfine frequency,  $f_{Rb} = \frac{E_B - E_A}{h}$ . This behavior explains the origin of the "dip" in Figure 4-2.



- 4-2.2 Detailed Block Diagram / Support Electronics. Figure 4-5 functionally illustrates the physics package and associated circuitry that encompass the operation of the rubidium frequency standard.
- 4-2.2.1 Power Supply PCB (Assembly Drawing No. 70509-1). The power supply provides filtered and regulated voltage (20 VDC) to the M-100 electronics. It also provides filtered voltage to the lamp heater and an unregulated voltage to the resonator and crystal heater elements. A float regulator is provided to assure in-spec performance (if a ripple voltage is superimposed on the supply voltage) and feeds a clean voltage to the lamp thermostat. The resonator thermostat and crystal thermostat are operating directly off the input power. The electronic power is dependent on the input voltage to the power supply, however, current drain is nearly constant.
- 4-2.2.2 Crystal Oscillator PCB (Assembly Drawing No. 70512-2). The crystal oscillator PCB consists of a 10 MHz third overtone crystal oscillator, a buffer that provides the 10 MHz output frequency, and 10 MHz to the Synthesizer/Mutiplier PCB.
- 4-2.2.3 Synthesizer/Multiplier PCB (Assembly Drawing No. 70515-2). The synthesizer/multiplier is driven by a 10 MHz signal from the crystal oscillator PCB and is phase modulated by a 127 Hz signal from the servo PCB. Its 60 MHz output stage is amplitude modulated by a 5.3125 MHz signal synthesized from 10 MHz. The multiplier drives the step recovery (snap) diode which is part of the physics package (section 4-2.1). The multiplier PCB also contains the C-field adjustment components.
- 4-2.2.4 Servo PCB (Assembly Drawing No. 705-153-1). The primary function of the servo PCB is to lock the crystal oscillator to the atomic hyperfine transition. This is accomplished by amplification of the 127 Hz error signal from the photocell followed by synchronous rectification (demodulation) and subsequent integration which generates a DC error signal that is routed back to the crystal oscillator.

The servo also contains the 127 Hz modulation generator and the lock detector. Lock detection is similar to the 127 Hz detection (synchronous rectification) of the main loop, but at twice the modulation frequency (Figure 4-2 and section 4-2.1). In addition, the servo contains a sweep/search circuit that repetitively sweeps the output frequency of the crystal oscillator within 40 seconds over its entire trim range until atomic resonance can be detected and normal operation of the servo PCB can begin.

- 4-2.2.5 Physics Package. Refer to section 4-2.1.
- 4-3 DETAILED CIRCUIT DESCRIPTION. (Refer to Appendix for schematics and parts lists. Schematics contain key voltage levels.)
- 4-3.1 Resonator Assembly. (Schematic Drawing No. 70522-2). The function of the resonator assembly is to compare the multiplied and synthesized output frequency of the crystal oscillator to the ground-state hyperfine transition frequency of <sup>87</sup>Rb. It also provides a 127 Hz error signal to the servo board to lock the crystal frequency to the atomic transition.
- 4-3.1.1 Microwave Cavity. The microwave (resonator) cavity is constructed of silver plated copper and housed in a mu metal shield. It contains the rubidium resonance cell. The photocell is mounted on the lid of the cavity and placed behind the Rb glass cell, directly in the light path of the Rb spectral lamp. The step recovery diode with coupling loop and the condenser assembly are located at the other end of the cavity. Cavity temperature is maintained by the resonator thermostat (4-3.1.5). The C-field coil is wound on the outside of the copper cylinder. The lid on the cavity contains the photocell.
  - 4-3.1.2 Step Recovery Diode. The 60 MHz signal from the multiplier and the 5.3125 MHz from the VCXO are summed on the multiplier/synthesizer board and then applied to the step recovery diode. This diode, CRl, produces radiation having frequencies given by the expression (60 n + 5.3125 m) MHz, where n = a positive integer and m = an integer. The diode is part of a tuned coupling loop, tuned to the 114th harmonic of 60 MHz (n=114);

both are part of the microwave cavity that is tuned to the same frequency. The bandwidth of the microwave cavity assembly is wide in comparison with the bandwidth of the atomic transition (< 1 kHz), so that the atoms function as a narrow-band filter for the microwave signal.

- 4-3.1.3 Photocell. The DC component of the photocell current corresponds to the total light incident on the photocell CR2. The AC signal components result when a microwave field corresponding to the Rb hyperfine frequency is applied simultaneously with pumping light (Figure 4-2). This signal is amplified by the servo PCB. The input stage of the servo PCB is configured as a low-noise, current-to-voltage converter.
- 4-3.1.4 C-Field Coil. The C-field coil is wound on the microwave cavity and provides a DC magnetic field (the C-field) within the resonator cavity. This magnetic field allows fine tuning of the 10 MHz output frequency by shifting the Rb frequency hyperfine transition by the second order Zeeman effect. The "C-field" strength is determined by current from three sources:
  - FIXED: R37 on the synthesizer board (70516) supplies current directly to the coil, increasing the hyperfine frequency below the lower end of the trim range.
  - MANUALLY-ADJUSTABLE: The 20 turn frequency adjustment potentiometer, R35 on the synthesizer PCB, supplies an adjustable current to the C-field coil, fine tuning the output frequency over  $\pm 1 \times 10^{-9}$ .
  - TEMPERATURE/FREQUENCY COMPENSATION: The power to heat the microwave cavity increases approximately 60 mW for every degree centigrade decrease of the ambient temperature. This results in a current change through Q5 and Q6 which are part of the resonator assembly and through R21 on the resonator thermostat assembly (70522-2). The voltage across R21 is routed to R28 on the same assembly and to the C-field coil. R28 determines the degree of temperature compensation.

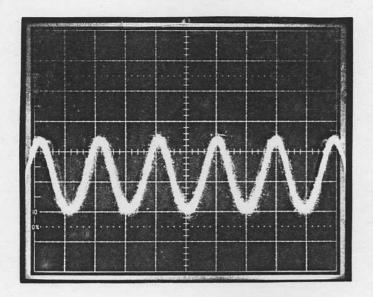
- 4-3.1.5 Resonator Thermostat Assembly. (Schematic Drawing No. 70522). The resonator (microwave cavity) thermostat maintains the temperature of the resonator precisely at the set temperature of approximately 75°C. This temperature assures proper Rb vapor pressure in the Rb resonance cell. The thermostat is of analog design. A thermistor senses the temperature of the microwave cavity, which holds the heater transistors Q5 and Q6 and acts as a heat spreader. Heater transistors Q1 and Q2 provide very efficient heating of the resonator since the voltage drop across is only about 300 mV (less than 1.5% of the supply voltage). Thermistor RTl is part of a balanced bridge circuit consisting of R2, R3, R7, R8, and the temperature select resistor R9. For a given resistance value of R9, the op amp will drive the resonator heaters until the desired temperature is attained. At this point, the bridge will be in a balanced condition. Operational amplifier Ul functions as an integrating amplifier, Ql and Q3 are emitter followers providing sufficient base current to the two heater transistors. During warm-up Q2 is turned on by the currentdependent voltage drop across R21 and the supply-voltage-dependent drop across R25 and R19. This feature eliminates the dependence of the warm-up time on the input voltage by providing nearly uniform warm-up power independent of supply voltage.
- 4-3.2 Lamp Assembly. (Schematic Drawing No. 70507) The lamp assembly consists of the lamp oscillator circuit, the lamp housing assembly, the lamp thermostat circuit and the rubidium lamp.
- 4-3.2.1 Lamp Oscillator. The lamp oscillator ignites and maintains an electrodeless plasma gas discharge in the rubidium lamp that is mounted inside the oscillator's tank circuit L3, C5. The oscillator is a modified Colpitts oscillator operating at approximately 85 MHz. The active element is the RF power transistor, 2N3375 (Q1).
  - C5 is adjusted for optimum lamp ignition characteristics. The remaining passive elements provide RF filtering for the power input and DC bias to the RF power transistor. L2 is one of the frequency determining elements of the Colpitts oscillator.

- 4-3.2.2 Lamp Thermostat. The lamp thermostat maintains the lamp housing temperature and therefore the lamp temperature at 115°C. It is configured as a linear temperature controller. Ul functions as the active gain element. Heater transistors Q5, Q6 and thermistor RTl are directly mounted to the lamp housing. Q2 and Q4 are emitter followers providing sufficient basedrive to the heater transistors. The maximum current during warm-up is limited by R28 and Q3. R29 and R25 change the maximum warm-up current as a function of the supply voltage, providing warm-up time independent of supply voltage changes.
- 4-3.3 Servo Board Assembly. (Schematic Drawing No. 705-154). The prime function of the servo circuit is to lock the crystal oscillator frequency to the "atomic reference". A secondary function is to provide a "Lock Monitor" for the user. These functions are accomplished by providing a 127 Hz modulation signal to the multiplier/synthesizer assembly and processing the signal from the photocell to provide a crystal-control voltage and the lock-monitor signal, respectively.

Refer frequently to the Block Diagram (Figure 4-5) and the Modulation Concept illustration (Figure 4-2) while reading this section.

4-3.3.1 Preamplifier. The signal from the photocell is on terminals E3 and E4. Ul is configured as a low noise current to voltage converter. If the lamp is ignited the DC voltage on Ul pin 6 is above 5 VDC, indicating normal operation of the Rb lamp. U2, pins 1, 2, and 3 function as an inverting amplifier with a gain of about 1000 and an upper corner frequency of less than 300 Hz.

The signal at TP1 (Figure 4-6) is for normal operating conditions a 254 Hz sinewave with a very small 127 Hz component. The nominal amplitude is between .2 and 1.5 Vpp. This signal is referred to as the TP1 signal.



If no hyperfine transition is detected, the maximum noise level on TP1 is less than 100 mVpp. Excessive noise can be caused by a noisy 20 VDC supply or a faulty lamp assembly as well as a noisy photocell or preamplifier U1 and will result in reduced short-term stability of the M-100.

Figure 4-6. TP1: .2V/DIV.; 2 ms Time/Div.

4-3.3.2 Reference Signal Generation. CMOS oscillator/divider U3 on the servo board provides the 127 and 254 Hz reference signals. The 127 Hz reference signal (TP5, Figure 4-7) is needed for synchronous rectification of the fundamental AC component of the photocell signal and for modulation of the microwave frequency. The 254 Hz reference signal is needed for synchronous rectification of the 2nd harmonic of the modulation signal, indicating atomic lock. The oscillator frequency of 8.128 kHz is determined by C17, R35 and select-in-test resistor R36. The divider portion of U3 divides the oscillator frequency into the required 127 and 254 Hz signals. The 127 Hz reference signal is routed from U3 pin 4 to pin 11 of synchronous demodulator U4, and also to the input of U6 pin 2 through the RC network R55, C28. The RC network R55, C28, in addition to the feedback network R56, C30 and the output RC filters (R57, R58 and C31 on the servo board; R3, C2, and C12 on the synthesizer board), serves to filter and phase shift the 127 Hz square wave signal to provide a sinusoidal voltage that is used to modulate the 60 MHz on the multiplier PCB.

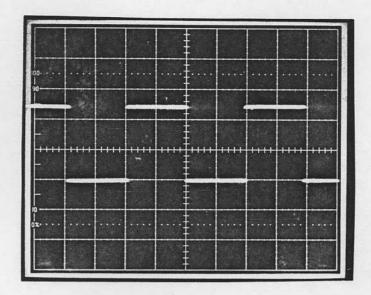


Figure 4-7. TP5: 5V/DIV; 2ms Time/DIV.

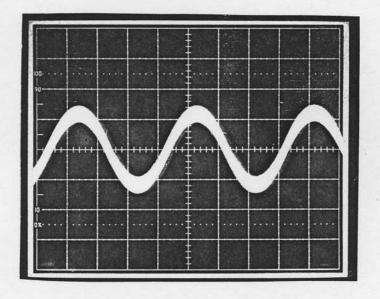


Figure 4-8. Test Point E8: 2V/DIV; 2 ms/DIV.

The 254 Hz reference signal is routed from U3 pin 5 to pin 9 of synchronous demodulator U4. The 254 and 127 Hz reference signals control the timing of the synchronous demodulators.

4-3.3.3 127 Hz Signal Processing. The preamplified photocell signal is applied to the notch filter U2 pin 12, 13, 14, which in turn provides a gain of approximately 80 for the 127 Hz signal component (TP2, Figure 4-9).

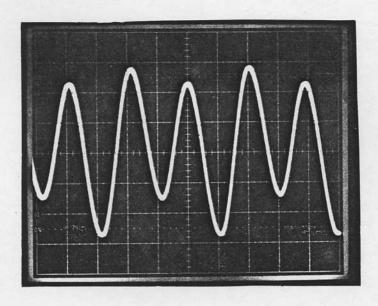


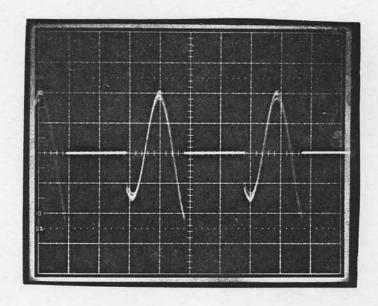
Figure 4-9. TP2: .5V/DIV.; 2ms Time/DIV.

Under normal operating conditions the signal at TP2 will have an amplitude of not less than 1 Vpp. The signal will appear as a 254 Hz sine wave, with a noticable 127 Hz component. The signal is then capacitively-coupled to the synchronous demodulator IC, U4 pin 12 where it is synchronously demodulated (rectified) by one of the three pairs of analog switches of U4. The output of the demodulator will show a positive or negative DC offset depending on the phase of the 127 Hz input signal (TP4, Figure 4-10).

If the crystal oscillator is locked to the hyperfine transition and does not require a change in its control voltage, the signal at TP4 (Figure 4-10) will be equal to the reference voltage (6.0 VDC nom) to the integrator.

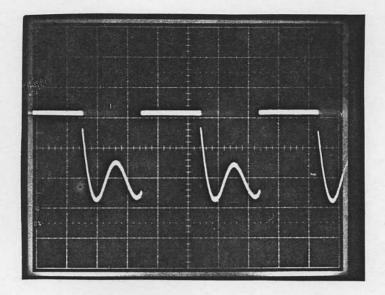
After passing through another CMOS switch, the signal is integrated by U5. The function of the other CMOS switch is outlined under "sweep circuit" in paragraph 4-3.3.4. The output voltage of U5 changes at a rate determined by the differential input voltage. As an example, an input differential of 500 mV causes an output voltage change of -500 mV per second. The changes will continue until the differential input is nulled by bringing the crystal back to center frequency, or until the op amp reaches its maximum output voltage. The output of integrator U5 is the crystal-control voltage that steers the frequency of the VCXO via a varactor diode (CR1, crystal oscillator PCB). A portion of the integrator output is also routed to the sweep control circuit at U6, pin 5. The crystal-control voltage can be monitored at the M-100 main connector, J1, pin F.

The following pictures in Figure 4-10 show the signal at TP4 for three different operating conditions. Frame A shows normal locked operation. Frames B and C show strong fundamental signals caused by frequency offsets of several parts in  $10^{-8}$ .

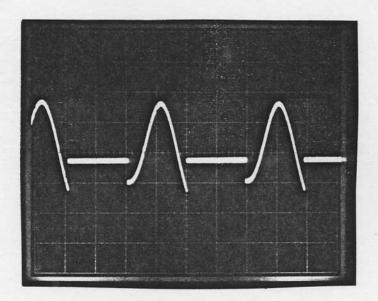


Frame A

Figure 4-10. TP4 Phase and Amplitude Characteristics (Sheet 1 of 2)



Frame B



Frame C

Figure 4-10. TP4 Phase and Amplitude Characteristics (Sheet 2 of 2)

4-3.3.4 Lock Circuit. The TPl signal is also amplified by the 254 Hz notch filter U6 pins 8, 9, and 10. The output of U6, pin 8 is then synchronously demodulated by the third pair of analog switches of U4 (TP7). If atomic lock exists, a negative DC offset on C33 will drive the output of U6, pin 14 high. R60, R62 provide a threshold of 200 mV for U6 to avoid triggering the lock indication by a marginal lock signal. Ql buffers the signal and generates the "Lock Monitor" signal at the M-100 output connector. U6, pin 14 also controls the sweep circuit.

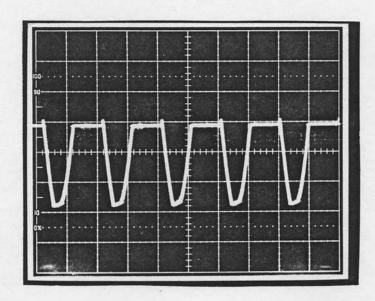


Figure 4-11. TP7: 2V/DIV.; 2 ms/DIV.

4-3.3.5 Sweep Circuit. In order to be able to compensate for several years of crystal aging in addition to frequency offsets of the crystal caused by environmental changes (e.g., temperature changes) the trim range of the oscillator is very wide compared to the width of the atomic resonance. To ensure lockup of the crystal, its frequency is swept over its trim range until atomic resonance can be detected.

This is accomplished by U4 connecting the integrator input (U5, pin 2) to U6, pin 7 as long as U6, pin 14 stays low (no atomic lock). U6, pins 5, 6, 7 functions as high hysteresis voltage comparator. The trigger points are controlled by R44 and R55 and the voltage reference. The lower trigger point is approximately 1.5 VDC, the higher trigger point is approximately 16 VDC. If the output of U5 is equal to or lower than the lower trigger point, U6's output becomes 0 VDC, resulting in a .7 V differential to the integrator. With R50 = 1 M and C22 = 1  $\mu$ F its output will rise .7 V/s until the upper trigger point of 16 VDC is reached. At this point, U6's output will go high, resulting in an approximate 1 VDC offset at the integrator input. This will decrease U5's output by 1 V/s, resulting in a sweep time of about 40 s. Due to the fast sweep, atomic resonance can be detected for only 100 ms at a time during each sweep cycle. Reliable transition from sweep to locked operation is facilitated by CR9.

- 4-3.4 Power Supply. (Schematic Drawing No. 70510). The internal power supply provides the unregulated voltages for the oscillator thermostat and the resonator thermostat. The supply voltage for the lamp thermostat is electronically filtered to improve the immunity to low frequency conducted interference. The supply also provides filtered and regulated voltage to all subassemblies of the M-100. The input voltage line is diode protected against reverse polarity inputs. A transient voltage suppressor of 1.5 KW peak power rating triggering at not less than 44 VDC protects the M-100 from power line spikes.
- 4-3.4.1 +20 Vdc Regulated Power Supply. The +20 vdc Power supply consists of Q1 thru Q9 and U1 along with their respective components mounted on the power supply board. Pass transistor Q9 is heat sinked to the frame assembly. Q1 and R7 limit the maximum supply current to approximately .5 A. The supply is set to  $(20 \pm .5 \text{ vdc})$ .

- 4-3.4.2 +21 Vdc Floating Power Supply. The floating power supply consists of Q10 through Q16 and supplies the lamp thermostat. In normal operation its output voltage is 5 VDC less than its input voltage. During warm-up when maximum heater power is demanded, its output is within 2 VDC of its input voltage.
- 4-3.5 Crystal Oscillator (VCXO) Assembly. (Schematic Drawing No. 70513).

  The function of the 10 MHz oscillator is to provide a clean 10 MHz signal at the M-100 output. The 10 MHz signal is also multiplied, as well as synthesized to 5.3125 MHz. The VCXO is temperature controlled and operated at the turning point of the crystal to improve short-term stability and to limit its maximum frequency deviation due to changes in the ambient temperature well inside its trim range.
- 4-3.5.1 Crystal Oscillator. The crystal oscillator consists of Y1, a 10 MHz 3rd overtone AT-Cut crystal, Q2 as the oscillator transistor, Q1 as the first Buffer stage and Q3 providing automatic gain control. Variable capacitor CR1 with C3 and C4 fine tune the oscillator frequency over approximately  $1.5 \times 10^{-6}$  as the tuning voltage changes from 1.5 to 16 VDC. C5 and C6 set the center frequency, however changing the center frequency will affect the trim range and vice-versa. Generally, an increase in center frequency will increase the trim range.

C10, L6 and L2 are set above the fundamental mode of the crystal and prevent oscillation of the crystal in this mode. C9 and T1 are tuned to 10 MHz.

The automatic gain control can be checked at TP3 using a DVM. The nominal voltage is around 1.1 VDC. This voltage will increase to > 2 VDC if Q3 fails or if insufficient amplitude is generated by the oscillator.

- 4-3.5.2 Fault Location, Crystal Buffer Section. The crystal buffer is part of the oscillator assembly and consists of Q4, Q5 and Q6. It is driven by a 10 MHz signal of 1 to 1.5 Vpp at TP4. Since Q4 is an emitter follower, the signal amplitude at TP5 is about 95% of the TP4 amplitude. Q5 provides about 2 Vpp drive to Q6 which in turn drives the primary of transformer T3. This transformer is tuned to 10 MHz and transforms the output impedance of Q6 to approximately 50 ohms (E7). Q4's collector drives T2 which is tuned to 10 MHz. The secondary of T2 provides about 3 Vpp to the multiplier (E5).
- 4-3.5.3 Crystal Thermostat. The analog thermostat maintains the crystal at its upper turning point of approximately 80°C. Thermistor RT1 (27K ohm nominal at 25°C) is mounted on the thermostat assembly which houses crystal Yl and is heated by Q10. RT1 is part of the bridge circuit consisting of R29, R30, R31, R32 and select resistor R33. The latter is selected for the bridge to be in a balanced condition when the operating temperature is reached. Ul is the active gain element of the loop, Q7 and Q9 are emitter followers providing base drive to the heater transistor Q10.

During warm-up the maximum heater current is limited by Q8, which is turned on by the voltage drop across R48 and R47. The voltage drop across R48 is almost entirely dependent on the heater current. The voltage across R47 is a function of the supply voltage. This feature eliminates the dependence of the warm-up time on the supply voltage. A functional check of this circuit can be performed by increasing the supply voltage to the M-100 while the heater is in a current-limiting mode. An increase of 20% of the voltage will result in approximately a 20% decrease of the heater current.

4-3.6 Synthesizer A5. (Schematic Drawing No. 70516). Synthesizer assembly (A5) contains the multiplier section and the synthesizer section in addition to the C-Field tuning elements.

4-3.6.1 Multiplier. The 10 MHz signal from the crystal oscillator is applied to the input of a frequency tripler consisting of Q3, Q4, and associated circuitry. C9 and L3 are tuned to 30 MHz, R12 limits the Q of the tank to about 30. The 30 MHz signal is capacitively coupled through C13 to transformer T1. At this point, the 127 Hz from the servo assembly modulates the rf signal via varactor CR6. The interaction of CR6 with the tuned tank circuit on the primary of T1 serves to phase modulate the rf at a 127 Hz rate. The secondary of T1 is center tapped to provide a split phase signal which drives the bases of Q5 and Q6. The result is a 60 MHz signal which is amplified by Q7, Q8. C17-L5; C20-L8 and C27-L10 are tuned to 60 MHz. Q7 and Q8 are class A inverting amplifiers. The 60 MHz signal at E6 drives the snap diode in the physics package through a coax cable. C27, C29 match the coax-cable to the driver stage. R31 and R34 provide the bias voltage for the snap diode.

#### NOTE .

All LC circuits are of low Q and retuning during the life cycle of the M-100 is not necessary, except if components need replacement. Change of select resistors R31 or R34 change the microwave level in the cavity. Retuning requires experience and should be done with the internal crystal oscillator held at  $\pm$  5x10<sup>-9</sup> of center frequency. The test point TP1 on the Servo PCB should be monitored with a scope and R31 or R34 should be selected for a broad maximum signal on TP1.

Any change of R31, R34 may change the temperature coefficient of the M-100. Typical values of R31 plus R34 are 400 to 2100 ohm.

- 4-3.6.2 Synthesizer. A portion of the 10 MHz signal from the crystal oscillator is applied to the base of Q2. Q2 converts the sinewave to a TTL compatible trigger signal. Power for the TTL circuits is provided by the voltage regulator VR1. VR1 is a 3 pin, +5V regulating IC. The 10 MHz TTL signal is divided down by U2 and U3 to 312.5 KHz. U1 is configured as an exclusive OR GATE and mixes the 312.5 KHz and the 5 MHz signals, resulting in a TTL signal of 4.6875 and 5.3125 MHz. The 4.6875 MHz component is suppressed by L11, C30 tuned to the upper TTL frequency. The 5.3125 MHz signal is mixed with the 60 MHz output of Q8, and routed to the step recovery diode in the resonator circuit, (paragraph 4-3.1.2).
- 4-3.6.3 C-Field Tuning. The C-Field tuning is outlined in detail in section 4-3.1.4.

# CHAPTER 5 MAINTENANCE, TROUBLESHOOTING AND REPAIR

- 5-1 INTRODUCTION. This chapter provides detailed procedures and instructions for performing all maintenance and repair functions on the M-100, including incoming acceptance tests, performance tests, calibration, troubleshooting and repair. Throughout the test procedures the M-100 will be referred to as the UUT (Unit Under Test).
- 5-2 REQUIRED TEST EQUIPMENT. The required test equipment to properly service the UUT is listed in Table 5-1. Test equipment other than the items listed may be used provided that they meet or exceed the Minimum Use Specification stated in Table 5-1. In the event that the required test equipment or a suitable substitute is not available it is recommended that the unit be returned to Efratom for service.

Table 5.1 REQUIRED MAINTENANCE TEST EQUIPMENT

#	Item	Minimum Use Specification	Test Equipment
5.1	DC Power Supply	Voltage: 0 to 30 vdc Accuracy: Output monitored Current: 0 to 3 adc	Hewlett Packard 6296A or 6433B
5.2	Digital Multimeter (DMM) (2 required)	Voltage: 0 to 30 vdc Accuracy: + 1.25% Current: 0 to 3 adc Resistance: 200 ohm range	John Fluke 8600 opt 01
5.3	Optional Reference Frequency Standard	Output: 10 MHz Accuracy: 5x10 <sup>-12</sup> Stability: parts in 10 <sup>12</sup>	1. EFRATOM RGR 2. Cesium Standard 3. EFRATOM H-Maser 4. EFRATOM MVLF
5.4	True RMS Voltmeter	Range: 0 to 1 vrms Input Frequency: 10 MHz Accuracy: <u>+</u> 3%	Hewlett Packard 3403C

#	Item	Minimum Use Specification	Test Equipment
5.5	Spectrum Analyzer	Range: 20 Hz to 100 MHz Bandwidth: 300 KHz	Hewlett Packard 141T Display with 8552 IF section and on 8553B RF section
5.6	Strip Chart recorder	Span Range: 1 mV to 1 V	Hewlett Packard 7132A or Texas Instruments PRIMA16AFR
5.7	Oscilloscope	Range: DC to 100 MHz	Tektronix 465 or 7704 MOD 129F with 7A26 Vert. P/I and 7B53A Time Base P/I
5.8	Resistive Load	Type: Feedthrough Impedance: 50 ohm Accuracy: + 0.5 ohm	Pomona Electric 4119-50 or Hewlett Packard 10100A
5.9	Atomic Oscillator Test Set	Int. Ref. Freq.: 10 MHz Accuracy: + 1X10 <sup>-11</sup> Stability: Parts in 10 <sup>12</sup>	Efratom TS105 or TS-105A
5.10	Phase Noise Test Set	Input Frequency: 10 MHz Bandwidth: > DC to 25 KHz from carrier	Efratom Model MNT

5-3 TEST PROCEDURES. The test procedures described in subsections 5-6 through 5-11 can be used to check performance for incoming inspection and periodic unit evaluation. These tests can be performed without removing the unit's outer cover. Calibration of the M-100 is accomplished by performing the tests described in Chapter 3, in addition to sections 5-6 through 5-16.

5-4 TROUBLESHOOTING. In the event that a major section or the complete unit is inoperative, troubleshooting and/or repair will be necessary. Flowcharts at the end of this chapter will isolate the fault and provide instructions for repair. In general, internal adjustments have only a limited range and are designed to compensate for minor variations in circuit components; seldom, if ever, will an internal adjustment restore operation. The test procedures in subsection 5-6 through 5-13 will serve as an aid in further isolating a trouble to a specific circuit section.

Since the operation of some circuits is dependent on proper operation of other circuits, troubleshooting must be performed in proper flowchart sequence. If the trouble indicates a possible malfunction of a specific board, perform the troubleshooting procedure on that board. If the problem is found to be in the physics package return the unit to the factory. The physics package is not field repairable.

5-5 EQUIPMENT HISTORY. It is recommended that an Equipment History be maintained for each unit, so that the results of the performance tests can be made a part of the permanent record for the Equipment History. A blank sample Performance Check List is included at the end of this section for your convenience. The blank sample check list may be reproduced as necessary to provide a permanent record.

5-6 WARM-UP CURRENT, FREQUENCY ACCURACY AND INPUT POWER TESTS.

5-6.1 Connect the equipment as shown in Figure 5-1.

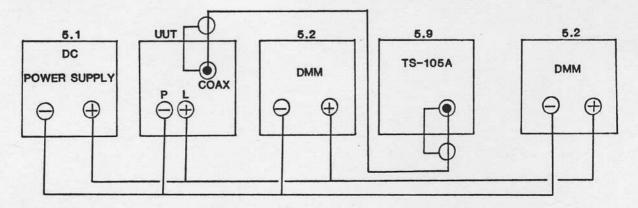


Figure 5-1. Warm-up Current, Frequency Accuracy, and Input Power Test Configuration.

- 5-6.1.1 Set the DMM #1 controls for voltage measurements in the 30 vdc range.
- 5-6.1.2 Set the DMM #2 controls for current measurements in the 3 adc range.
- 5-6.1.3 Ensure that all test equipment is operating and has had sufficient warm-up time.
- 5-6.2 Adjust the DC power supply controls to obtain a  $26 \pm 1.3$  vdc indication on DMM #1. Note the exact indication; it will be required in step 5.6.6.
- 5-6.3 Allow the UUT to operate at ambient temperature for at least five hours.

The maximum temperature fluctuation must not exceed  $\pm 2^{\circ}$ C. Also, continuous operation of the atomic oscillator test set is preferred over warm-up.

- 5-6.4 Ensure that the atomic oscillator test set has been operating at ambient temperature for at least two hours, press the RESET push button to begin the test.
- 5-6.5 Allow the atomic oscillator test set sufficient time to display the UUT Offset for the 100 seconds averaging time.
- 5-6.6 Record the UUT offset as indicated on the atomic oscillator test set. If the indicated offset is greater than ± 5x10<sup>-11</sup>, adjust the UUT Frequency Trim potentiometer (as described in Chapter 3), to obtain an in-tolerance indication. If an in-tolerance indication is not possible and the UUT frequency is too low, perform section 5-14; if the UUT frequency is too high, perform subsection 5-15.
- 5-6.7 Adjust the DC power supply for minimum output (0 vdc), and note the turn-off time. Allow a minimum of two hours before proceeding.
- 5-6.8 Monitor DMM#1 and DMM #2 while adjusting the DC power supply for the exact voltage noted in step 5-6.2, and note the turn-on time.

5-6.9 Record the DMM #2 maximum current indication during the UUT 10 minute warm-up period.

NOTE

The UUT current normally reaches maximum within 2 minutes after input power is applied.

- 5-6.10 Verify that the UUT maximum warm-up current is  $\leq$  2.2 adc.
- 5-6.11 At the end of the 10 minute warm-up, press the atomic oscillator test set RESET push button and record the UUT frequency offset for 100 seconds averaging times.
- 5-6.12 Verify that the UUT frequency offsets recorded for steps 5-6.6 and 5-6.11 differ by no more than  $\pm 2 \times 10^{-10}$ .
- 5-6.13 Allow the UUT to operate continuously for at least 1 hour.
- 5-6.14 Note the voltage indication on DMM #1 and the current indication on DMM #2.
- 5-6.15 Using the following formula and the data from step 5.6.14 determine the UUT power comsumption.

Power Formula: P = I E

Where: P = Power

I = Current

E = Input voltage

- 5-6.16 Verify that the UUT power consumption after > 1 hour operation is  $\leq$  18 watts.
- 5-6.17 If no other tests are required, adjust the DC power supply for minimum output and disconnect the test setup.

- 5-7 SHORT-TERM STABILITY (Allan Variance).
- 5-7.1 Ensure that the equipment is connected as shown in Figure 5-1, (DMM #2 is not required for this test).
- 5-7.2 Adjust the DC power supply controls to obtain a 26  $\pm$  1.3 vdc indication of DMM #1.
- 5-7.3 Ensure that the UUT and the Atomic Oscillator Test Set have had sufficient stabilization time. (The UUT requires 1 hour stabilization).

The maximum temperature fluctuation must not exceed  $\pm 2$  °C.

- 5-7.4 Press the RESET push button on the Atomic Oscillator Test Set to begin the Allan Variance tests.
- 5-7.5 Allow the Atomic Oscillator Test Set sufficient time to display the Allan Variance for averaging time of 1 and 10 seconds.
- 5-7.6 Verify that the Allan Variance for 1 second averaging time is  $\leq 3 \times 10^{-11}$ , and that the Allan Variance for 10 seconds averaging time is  $\leq 1 \times 10^{-11}$  as indicated on the atomic oscillator test set.

#### NOTE

If the UUT is not within the stated tolerance it may be necessary to continue the test in order to obtain a 100 second averaging time indication. If a 100 second averaging time indication is required the tolerance is  $\leq 3 \text{x} 10^{-12}$ .

- 5-7.7 If no further tests are required, adjust the DC power supply for minimum output and disconnect the test setup.
- 5-8 TRIM RANGE TEST.
- 5-8.1 Ensure that the equipment is connected as shown in Figure 5-1, (DMM #2 is not required for this test).

- 5-8.2 Adjust the DC power supply controls to obtain a 26  $\pm$  1.3 vdc indication of the DMM #1.
- 5-8.3 Ensure that the UUT and the atomic oscillator test set have had sufficient time to stabilize. (The UUT requires 1 hour to stabilize).
- 5-8.4 Determine the UUT nominal output frequency from the Atomic Oscillator Test Set's Frequency Offset indication.
- 5-8.5 Locate the UUT frequency adjustment screw access hole (refer to Chapter 3, Figure 3-4 if necessary) and remove screw.
- 5-8.6 Using the appropriate adjustment tool, rotate the UUT trim potentiometer fully clockwise and verify that the frequency offset indication on the test set increases  $\geq 1 \times 10^{-9}$  of the nominal output. Record the shift from the nominal.
- 5-8.7 Rotate the UUT trim potentiometer fully counter clockwise and verify that the frequency decreases  $\geq 1 \times 10^{-9}$  of the UUT nominal output. Record the shift from nominal.
- 5-8.8 Using the following formula and the data recorded in steps 5-8.6 and 5-8.7, compute the UUT trim range.

Trim range (
$$\triangle f/f$$
 range) =  $\triangle f/f$  Max +  $\triangle f/f$  Min

Where:  $\triangle f/f$  Max =  $\frac{f \text{ max } - f \text{ (test set ref)}}{f \text{ (test set reference)}}$ 

$$\triangle f/f \text{ Min = } \frac{f \text{ (test set ref)} - f \text{ min}}{f \text{ (test set reference)}}$$

- 5-8.9 Verify that the UUT trim range is  $\geq 3 \times 10^{-9}$ .
- 5-8.10 Adjust the UUT trim potentiometer to a position which returns the UUT as close to 10 MHz as possible  $\pm$  5x10<sup>-11</sup>. Replace screw in access hole.

- 5-9 OUTPUT LEVEL TEST.
- 5-9.1 Connect the equipment as shown in Figure 5-2.

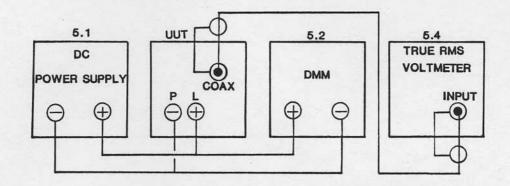


Figure 5-2. Output Level Test Configuration.

- 5-9.2 Adjust the DC power supply output controls to obtain a  $26 \pm 1.3$  vdc indication on the DMM.
- 5-9.3 Allow a minimum of 10 minutes warm-up time for the UUT.
- 5-9.4 Verify that the UUT output level as indicated on the RMS voltmeter is between 0.45 and 0.65 VRMS.
- 5-10 HARMONIC/NON-HARMONIC DISTORTION TESTS.
- 5-10.1 With the equipment connected as shown in Figure 5-2, disconnect the RMS voltmeter, and connect the UUT output to the spectrum analyzer input.
- 5-10.2 Set the spectrum analyzer controls for 100 MHz sweep 300 KHz bandwidth.
- 5-10.3 Adjust the 10 MHz fundamental to REF on the spectrum analyzer display.
- 5-10.4 Measure the highest amplitude harmonic (in dB) below the REF.
- 5-10.5 Verify that the UUT Harmonic Distortion is at least 30 dB down from reference.
- 5-10.6 Measure the highest amplitude on Non-Harmonic signal up to 90 MHz.
- 5-10.7 Verify that the Non-Harmonic Distortion is at least 80 dB from the reference.

#### 5-11 LONG-TERM STABILITY TEST.

Long-term stability refers to slow changes in the average frequency over time, due to secular changes in the UUT physics and/or electronic circuitry. Using the test set-up provided in Figure 5-3, it is recommended that daily readings be taken from the Efratom TS-105A and plotted graphically to estimate long-term drift (aging). Measurement periods should be a minimum of 30 days to obtain meaningful results. It is also important that the daily readings are taken at approximately the same time to minimize the effects of temperature fluctuations.

#### NOTE

During long-stability testing, the UUT should be placed in an environment with stable temperature, barometric pressure, and magnetic fields. Refer to specifications to estimate effects of environment on stability. Also ensure that the UUT has been operating 14 days continuously prior to the test.

- 5-11.1 With the equipment connected as shown in Figure 5-3, and the required stabilization time allowed, press the test set's RESET pushbutton to begin the test.
- 5-11.2 Allow sufficient time for the test set to display the data required and begin recording readings daily. After a minimum of 30 readings are plotted graphically, verify that the UUT long-term stability is within the tolerance listed in Table 1-1, SPECIFICATIONS.

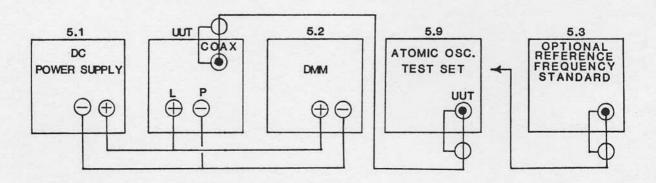


Figure 5-3. Long-Term Stability Test Setup.

5-12 VOLTAGE VARIATION TEST

5-12.1 Connect the equipment as shown in Figure 5-1.

NOTE

The ambient temperature should not vary more than  $\pm$  1°C during performance of this test.

- 5-12.2 Adjust the DC power supply controls to obtain a 26 + 0.1 vdc.
- 5-12.3 Allow the UUT and the Atomic Oscillator Test Set sufficient time to stabilize (the UUT requires 1 hour min.).
- 5-12.4 At the end of the stabilization period, determine and record the UUT output frequency.
- 5-12.5 Adjust the DC power supply controls to obtain a 28.6 ± 0.1 vdc indication on the DMM. Allow the UUT to operate at this input voltage for at least 15 minutes. Determine and record the UUT output frequency.
- 5-12.6 Adjust the DC power supply controls to obtain a 23.4 ± 0.1 vdc indication on the DMM. Allow the UUT to operate at this voltage for at least 15 minutes. Determine and record the UUT output frequency.
- 5-12.7 Adjust the DC power supply controls to obtain  $26 \pm 0.1$  vdc indication on the DMM. Allow the UUT to operate at this input voltage for at least 15 minutes and record the UUT output frequency.
- 5-12.8 Calculate the average reference frequency by utilizing the following formula:

$$f = \underline{f(\text{from step } 5-12.4) + f \text{ (from step } 5-12.7)}}_{2}$$

5-12.9 Verify that the frequencies obtained in steps 5-12.5 and 5-12.6 are within  $+ 1 \times 10^{-11}$  of the reference frequency obtained in step 5-12.8.

- 5-13 CRYSTAL AGING COMPENSATION.
- 5-13.1 If the crystal control voltage approaches the end of it's range (+2 to +15 vdc), a correction of the crystal oscillator base frequency must be made.
- 5-13.1.1 Connect the equipment as shown in Figure 5-4, but do not make the dotted-line connection until instructed to do so.

#### CAUTION

If the UUT output frequency is  $\geq 10.000050$  MHz after normal warm-up times, a check of the crystal thermostat at ambient temperature is mandatory. DO NOT attempt to reset crystal trim range as if this condition exists, the adjustment will

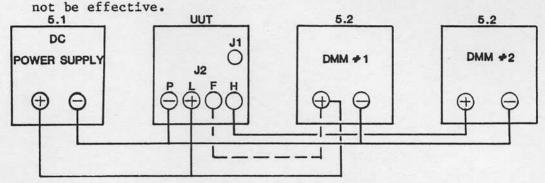


Figure 5-4. Crystal Aging Compensation Test Setup.

- 5-13.1.2 Set DMM #1 controls to measure dc voltage in the 30 vdc range, and DMM #2 to 200 ohm range. (Do not use auto range for this test).
- 5-13.1.3 Adjust the DC power supply output for a  $26 \pm 1.3$  vdc indication on the DMM #1,
- 5-13.1.4 Disconnect the DMM #1 positive (+) lead connected to the DC power supply positive output connector. (Do not disturb the positive input to UUT).
- 5-13.1.5 Set the DMM #1 controls to measure DC voltage in the 20 volt range, and connect the positive lead to the UUT J2 pin F connection.
- 5-13.1.6 After the UUT has operated a minimum of 1 hour, ensure that DMM #2 indicates 120 ohm and maintains this indication throughout the remainder of the test. (This indicates that the UUT has locked onto the atomic resonance frequency.)

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5-13.1.7 Refer to Figure 5-5 to locate the UUT crystal trim adjustment (C5).

Remove screw to access crystal trim adjustment.

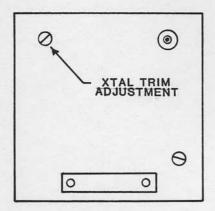


Figure 5-5. Crystal Trim Adjustment Location.

- 5-13.1.8 Using the proper adjustment tool or insulated screwdriver, slowly rotate the crystal trim adjustment to obtain a voltage indication, on DMM #2, of +9 vdc (+ 1V). Clockwise rotation decreases the control voltage, counterclockwise rotation increases the control voltage.
- 5-13.1.9 If the crystal control voltage cannot be adjusted to +9 volts ( $\pm$  1V) with the crystal trim adjustment proceed with step 5-13.2.
- 5.13.2 Remove the UUT outer cover by first removing the twelve (12) screws and related washers from the outer cover sides near the baseplate end of the UUT. The remove the four (4) screws and related washers from the connector end of the outer cover. Carefully slide the UUT out of the outer cover.

#### NOTE

The UUT comes supplied with either one (1) or two (2) spare capacitors to be used as necessary to compensate for crystal aging. The number of capacitance value(s) has been determined by the preselected value of C6 on the oscillator board. The compensation capacitors are designated A4C6+ and A4C6- (if two were necessary) and are located on the synthesizer board assembly. Refer to the final assembly drawing, Drawing No. 70500-1, top cut-away and Note (5) for further information and physical location. If the crystal control voltage was found to be too low (<+2 vdc) perform section 5-13.3, if the crystal control voltage was found to be too high (>+15 vdc) perform section 5-13.4.

- 5-13.3 Locate C8 on the oscillator board assembly. Refer to Drawing No. 70512-2.
- 5-13.3.1 Locate and remove adjustment capacitor A4C6+ from the synthesizer board assembly.
- 5-13.3.2 Connect the adjustment capacitor in parallel to C8 on the oscillator board.
- 5-13.3.3 Ensure that the crystal trim adjustment C6 is set to the center of its range.
- 5-13.3.4 Using the method described in steps 5-13.1.1 through 5-13.1.9 readjust the control voltage to 8 vdc (+ 1V).
- 5-13.4 Locate C6 on the oscillator board assembly. Refer to Drawing No. 70512-2.
- 5-13.4.1 Locate and remove adjustment capacitor A4C6- from the synthesizer board assembly.
- 5-13.4.2 Remove C8 from the oscillator board and connect A4C6- in its place.
- 5-13.4.3 Ensure that the crystal trim adjustment C6 is set to the center of its range.
- 5-13.4.4 Using the method described in steps 5-13.1.1 through 5-13.1.9 readjust the control voltage to 8 vdc (+ 1V).
- 5-13.4.5 Secure the UUT outer cover by reinstalling all of the screws and washers.

If during the performance of Chapter 3, Operational Frequency Accuracy Test, or section 5-6 in this chapter (Frequency Accuracy portion), it was found that the Frequency Adjust potentiometer (R35) did not have sufficient range to adjust the UUT output frequency within the required  $5 \times 10^{-11}$  it will be necessary to adjust the C-field current through the resonator coil.

An increase in C-field current will increase the UUT output frequency, whereas decreasing the C-field current will decrease the output frequency. Refer to synthesizer assembly Drawing No. 70515-2 and synthesizer schematic Drawing No. 70516 to facilitate the correction compensation. If the UUT output frequency was found to be too low after adjusting the UUT frequency, adjust potentiometer R35 fully clockwise and perform the required steps in section 5-14. If the UUT output frequency was found to be too high after adjusting R35 fully counterclockwise, perform section 5-15.

- 5-14 UUT OUTPUT FREQUENCY LOW COMPENSATION.
- 5-14.1 Remove the UUT from its cover by removing the twelve (12) screws and related washers from the outer cover sides near the baseplate end of the UUT. Then remove the four (4) screws and related washers on the connector end and carefully slide the UUT out of the outer cover.

NOTE

The C-field current is adjusted by changing pre-selected jumper wires on the synthesizer board assembly. Refer to Figure 5-6.

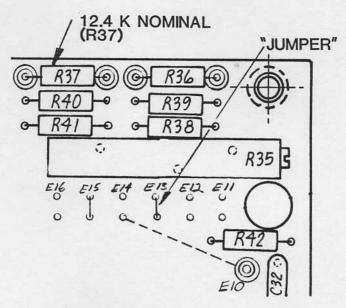


Figure 5-6. Location of Frequency Correction Compensation Jumpers on Synthesizer Board Assembly.

5-14.2 Locate the compensation jumper connections on the synthesizer board. NOTE

Terminal El5 is normally jumpered to El0 at the factory, (dotted-line connections in Figure 5-6). On some UUT's the jumper was not required. If the UUT does not have a jumper between El0 and either El6, El5, or El4, perform section 5-14.3. If a jumper is connected between El0 and either El6 or El5, perform 5-14.4. If El0 is jumpered to El4, perform section 5-14.5.

- 5-14.3 Using a 35 to 40 watt soldering iron and SN63WRMAP3 solder, (Federal Specification QQ-S-571E), perform the following:
- 5-14.3.1 Locate terminal E16 and the corresponding E10 connection on the synthesizer board, refer to Figure 5-6.
- 5-14.3.2 Select a piece of uninsulated 24 gauge wire approximately 1/8 inch long.
- 5-14.3.3 Lay the jumper across the El6 and corresponding El0 terminals, and carefully solder the jumper in place.

- 5-14.3.4 Replace the UUT outer cover and secure with four (4) of the screws removed in step 5-14.1.
- 5-14.3.5 Perform the steps in section 3-9 to adjust and verify that the UUT output frequency is 10 MHz  $\pm$  5x10<sup>-11</sup>.
- 5-14.3.6 Secure the UUT cover by reinstalling all of the remaining screws removed in step 5-14.1.
- 5-14.4 Using a 35 to 40 watt soldering iron and SN63WRMAP3 solder (Federal Specification QQ-S-571E), perform the following:
- 5-14.4.1 Remove the existing jumper between E10 and either E16 or E15 terminals.

Moving the jumper from E10/E16 to E10/E15 or E10/E15 to E10/E14 will increase the UUT output frequency by approximately  $1 \times 10^{-9}$ .

- 5-14.4.2 Select a piece of uninsulated 24 gauge wire approximately 1/8 inch long.
- 5-14.4.3 Lay the jumper across the E10/E15 or E10/E14 terminals as illustrated in Figure 5-7 and carefully solder the jumper in place.
- 5-14.4.4 Replace the UUT cover with four (4) of the screws removed in step 5-14.1.
- 5-14.4.5 Perform the necessary steps in section 3-9 to adjust and verify that the UUT output frequency is 10 MHz  $\pm$  5x10<sup>-11</sup>.
- 5-14.4.6 Secure the UUT cover by reinstalling all of the remaining screws removed in step 5-14.1.
- 5-14.5 If it was found that the E10/E14 terminals have a jumper installed it will be necessary to recalculate the value of R37 and replace the old R37 with a resistor of the new calculated value. Proceed as follows:

- 5-14.5.1 Locate and determine the value of R37 on the Synthesizer assembly. Refer to Appendix, Drawing No. 70515-2.
- 5-14.5.2 Calculate the new required value for R37 using the following formula:

R37 new = 
$$\frac{40}{\frac{\Delta f}{f} + \frac{40}{R37}}$$
 Original

Where:  $\frac{\Delta f}{f}$  = Anticipated positive frequency increase in parts of  $10^{-9}$ .

$$R37 = K Ohms$$

- 5-14.5.3 Using a 35 to 40 watt soldering iron and SN63WRMAP3 solder (Federal Specification QQ-S-571E), remove resistor R37 and the jumper across E10/E14.
- 5-14.5.4 Replace R37 with a resistor of the calculated value from step 5-14.5.2.
- 5-14.5.5 Replace the UUT cover and secure with the screws removed in step 4-15.1.
- 5-14.5.6 Perform the necessary steps in section 3-9 to adjust and verify that the UUT output frequency is 10 MHz  $\pm$  5x10<sup>-11</sup>.
- 5-14.5.7 Secure the UUT cover by reinstalling all of the remaining screws removed in step 5-14.1.
- 5-15 UUT OUTPUT FREQUENCY HIGH COMPENSATION.
- 5-15.1 Remove the UUT from its outer cover by removing the twelve (12) screws and washers from the outer cover sides located near the baseplate end of the UUT. Then remove the four (4) screws and related washers on the connector end and carefully slide the UUT out of the outer cover. The "C-field" current is adjusted by changing pre-selected jumper wires or recalculating the required value of R37 and replacing R37 if necessary. Locate the compensation jumper connections on the synthesizer board. Refer to Figure 5-7.

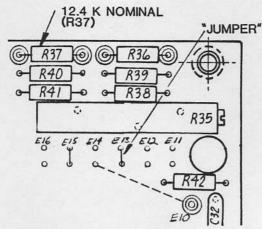


Figure 5-7 Location of Frequency Correction Compensation Jumper on Synthesizer Board Assembly.

Terminal E15 is normally jumpered to E10 at the factory, (dotted-line connections in Figure 5-7). If a jumper is installed between E10 and either E14 or E15 perform section 5-15.3. If a jumper is installed between E10 and E16 perform 5-15.4. (It may be also necessary to perform 5-15.5). If E10 is not jumpered to either E14, E15, or E16 perform section 5-15.5.

- 5-15.3 Using a 35 to 40 watt soldering iron and SN63WRMAP3 solder (Federal Specification QQ-S-571E) perform the following:
- 5-15.3.1 Select a piece of uninsulated 24 gauge wire approximately 1/8 inch long.
- 5-15.3.2 If E10/E14 are jumpered, remove the existing jumper and lay the new jumper wire across the E15 and corresponding E10 terminals. If E10/E15 are jumpered, remove the existing jumper and lay the new jumper wire across the E16 and corresponding E10 terminals.
- 5-15.3.3 Carefully solder the jumper wire in place.
- 5-15.3.4 Replace the UUT cover and secure with four (4) of the screws removed in step 5-15.1.
- 5-15.3.5 Perform the necessary steps in section 3-9 to adjust and verify that the UUT output frequency is  $10~\mathrm{MHz} + 5\mathrm{x}10^{-11}$ .

- 5-15.3.6 Secure the UUT cover by reinstalling all of the remaining screws removed in step 5-15.1.
- 5-15.4 If it was found that the E10/E16 terminals have a jumper installed, perform the following steps.
- 5-15.4.1 Using a 35 to 40 watt soldering iron, remove the jumper across the E10/E16 terminal.
- 5-15.4.2 Replace the UUT cover and secure with four (4) of the screws removed in step 5-15.1.
- 5-15.4.3 Perform the required steps in section 3-9 to adjust and verify that the UUT output frequency is 10 MHz  $\pm$   $5 \times 10^{-11}$ .
- 5-15.4.4 Secure the UUT cover by reinstalling all of the remaining screws removed in step 5-15.1.
- 5-15.5 If no jumper exists between ElO and El4, El5, or El6 it will be necessary to replace R37 with a recalculated valued resistor. To recalculate and replace R37 perform the following steps.
- 5-15.5.1 Calculate the required increased resistance value for R37 using the following formula:

R37 new = 
$$\frac{\Delta f}{f} + \frac{40}{R37 \text{ Original}}$$

Where:  $\frac{\Delta f}{f}$  = Anticipated negative frequency shift in parts of  $10^{-9}$ .

R37 = K ohms

- 5-15.5.2 Using a 35 to 40 watt soldering iron and SN63WRMAP3 solder (Federal Specification QQ-S-571E) remove the existing R37 resistor and install a new R37 resistor with the resistance value calculated in step 5-15.5.1.
- 5-15.5.3 Replace the UUT cover and secure with four (4) of the screws removed in step 5-15.1.

- 5-15.5.4 Perform the required steps in section 3-9 to adjust and verify that the UUT output frequency is  $10~\mathrm{MHz} \pm 5\mathrm{x}10^{-11}$ .
- 5-15.5.5 Secure the UUT outer cover by reinstalling all of the remaining screws removed in step 5-15.1.
- 5-16 PHASE NOISE TEST. Using the equipment setup in Figure 5-8, the Efratom MNT Phase Noise Test Set can be used to measure the "close-in" single side-band (SSB) phase noise  $[\mathcal{L}(f)]$  of the UUT. Refer to detailed procedure in the MNT manual for Calibration to the UUT and actual Phase Noise measurements.

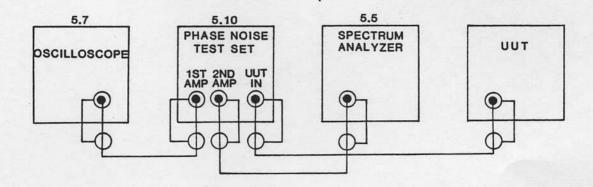


Figure 5-8. Phase Noise Measurement Test Set-up.

5-17 TROUBLESHOOTING AND REPAIR. A series of Fault Isolation
Flowcharts are provided to aid the technician in the repair of a
faulty board or part. The flowcharts are presented in logical
fault isolation order and must be performed in the proper sequence
given. The troubleshooting/repair procedures are designed to
isolate a fault in the resonator (physics package) as soon as
possible as this part of the M-100 is not field repairable. If
the fault isolation flowcharts lead to a physics package fault,
return the entire unit to Efratom for proper repair.

The fault isolation flowcharts are designed to quickly isolate the fault or adjustment. The technician is then referred to the detailed circuit description (chapter 4) and to the schematics following the flowcharts which include key voltages and indications for component troubleshooting and replacement. Using standard circuit tracing techniques, the detailed circuit descriptions, and key indications on schematics, the mean time to repair or adjust the unit is less than 1 hour.

### 5-17.1 TROUBLESHOOTING / REPAIR TURN-ON.

5-17.2 Remove the UUT outer cover by first removing the twelve (12) screws and related washers from the outer cover sides near the baseplate end of the UUT. Then remove the four (4) screws and related washers from the connector end of the outer cover.

Carefully slide the UUT out of the outer cover.

# 5-17.3 Connect the equipment as shown in Figure 5-9.

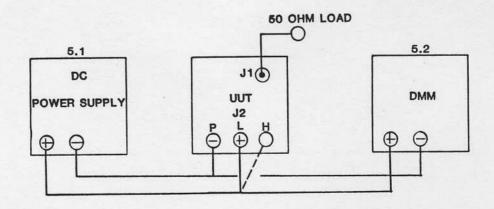


Figure 5-9. Troubleshooting / Repair Setup

- 5-17.4 Adjust the DC power supply controls to obtain a  $26 \pm 1.3$  vdc indication on the DMM. Allow the UUT a minimum of 10 minutes warm-up time.
- 5-17.5 Fault Isolation and Repair. When performing the troubleshooting procedures contained in the fault isolation flowcharts (Figures 5-10 through 5-14), it is suggested that the technician follow the troubleshooting/repair procedures contained in the flowcharts in the given sequence. Each question or procedure will narrow the possible functional area of fault and refer the operator to the appropriate repair, adjustment or realignment, as required. Once the flowcharts have isolated a specific board, the operator should refer to the proper schematic following the flowchart section. Each schematic illustrates key points on the board and their corresponding signal, amplitude and voltage levels. This information will isolate the board fault to a specific component part for replacement or adjustment.
- 5-18 REPAIR, REPLACEMENT, AND REASSEMBLY TESTING.
- 5-18.1 SOLDERING SUGGESTIONS. SN63WRMAP3 SOLDER, per QQ-S-571, and a 35 to 40 watt soldering iron should be used to accomplish the majority of the soldering done on the M-100. If a higher wattage soldering iron is used, excessive heat can cause the etched circuit wiring to separate from the board material.
- 5-18.2 HIGH FREQUENCY CONTACTS. If it becomes necessary to solder in the general area of any of the high frequency contacts in the unit, clean the contacts immediately upon completion of the soldering.

- 5-18.3 REPLACEMENT PARTS. The parts lists located in the appendix following this chapter contain information that identifies electrical and some mechanical components for the purpose of ordering replacement parts for the M-100. Each parts list includes the following information as a minimum under the column headings listed:
  - a. ITEM NO. The item numbers listed sequentially on each parts list.
  - b. QTY REQD. Indicates quantity of each item required for the applicable sub-assembly or assembly. A/R is an abbreviation for "as required".
  - c. PART OF IDENT NUMBER. This column indicates the MIL-SPEC, Efratom, or manufacturer's part number to be used when ordering required replacement components.
  - d. DESCRIPTION. Included in this column is a brief description of the part indicating the type of component as well as mechanical dimensions or electrical characteristics as applicable. All abbreviations used are in accordance with MIL-STD-12.
  - e. REFERENCE. Reference designators are listed in accordance with the applicable schematic and assembly drawing. This column also includes the manufacturers name as might be required to order replacement parts.
- 5-18.4 ORDERING INFORMATION. To procure replacement parts, address order to the Ball Corp., Efratom Division, Attn: Marketing Department. As a minimum the request shall include parts list number, item number, part number, and quantity required.
- 5-19 REASSEMBLY TESTING. The adjustments, repair, or alignments required in the fault isolation flowcharts (Figure 5-10 through 5-14) should be followed by the retesting of the procedure which led to the fault isolation to ensure the unit is functioning as required. Reassembly of the UUT can be accomplished by reinstalling the screws in reverse order from section 5-17.2. It is recommended that the operator subject the UUT to the checks in chapter 3 after repair or adjustments.

# FAULT ISOLATION SEQUENCE

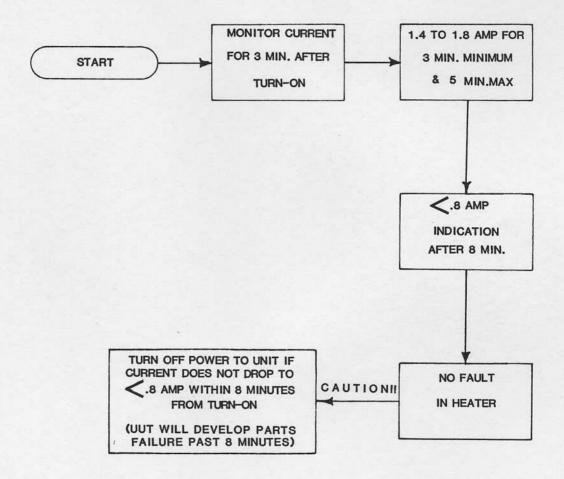
## A) GENERAL

- 1. Heater checks
- 2. Check power supply, if power supply is defective, repair and repeat heater check.
- 3. Warm-up as required.
- 4. Check Lamp Volts as required.
- 5. Check Crystal Trim Range as required.
- 6. Refer to Main Fault isolation flowchart.
- 7. Individual Fault Location.

## B) SPECIAL CONDITIONS

# 1. Normal lock indication after warm-up, No or low 10 MHz output signal Refer To Crystal Assy Buffer Section

- 2. Stable 10 MHz output (in-spec) Servo
  No lock indication Lock indication
- 3. Output frequency  $\geq$  10.000050 MHz Check Crystal Thermostat



5-26

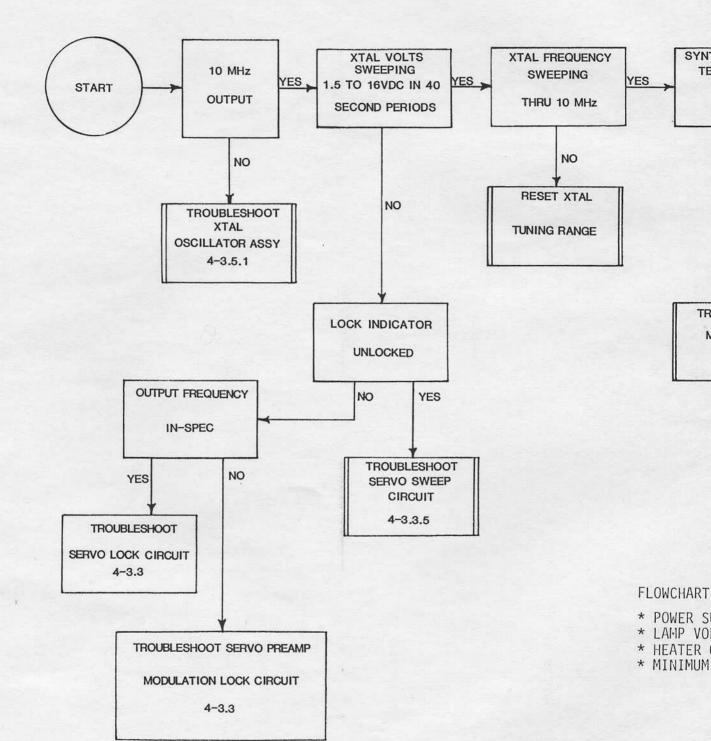
RETURN TO EFRATOM

RESET XTAL

TRIM RANGE

SEE NOTE

YES



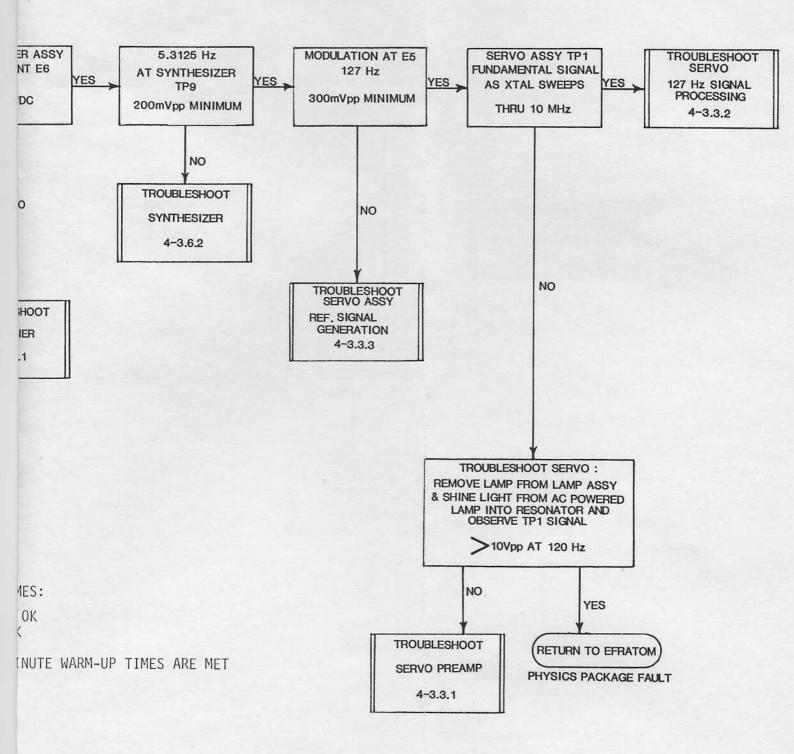
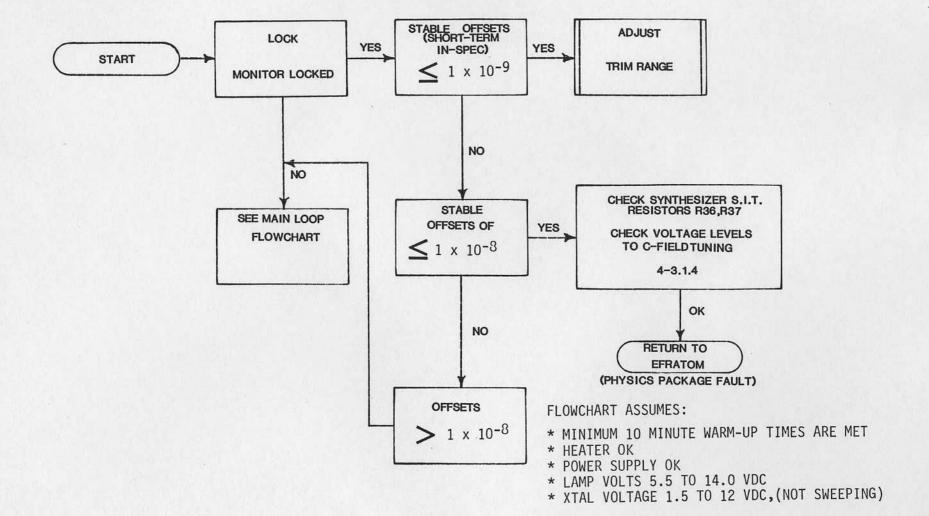


Figure 5-13. Main Fault Isolation Flowchart.



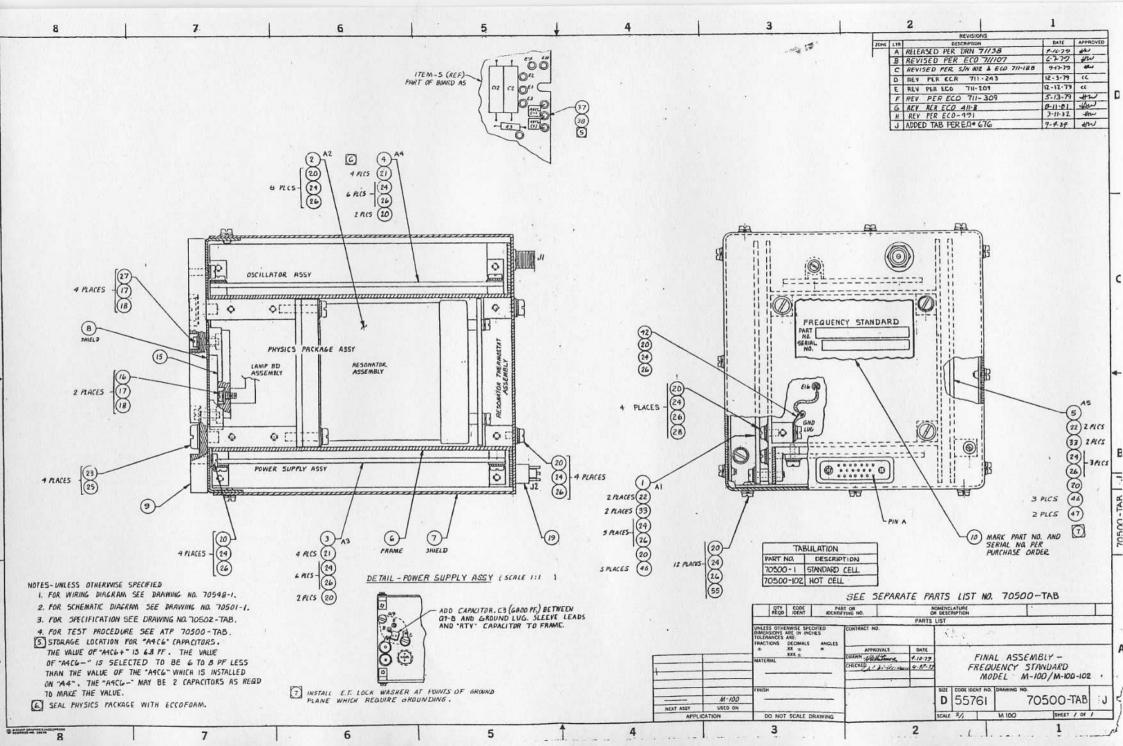
# APPENDIX A

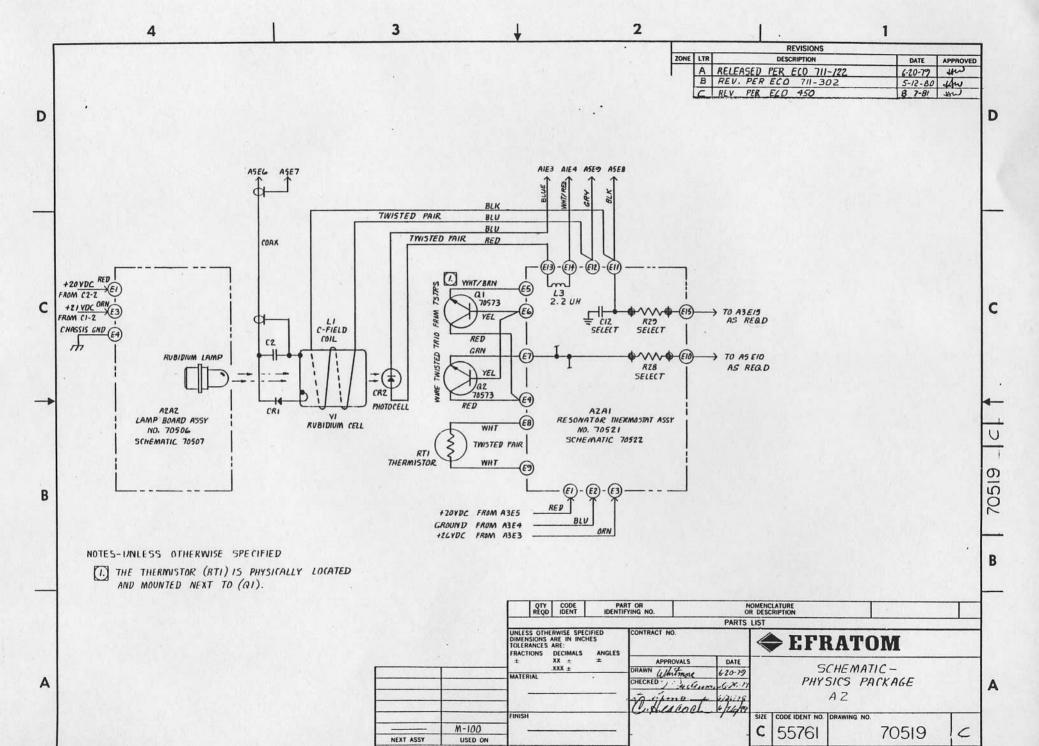
TROUBLESHOOTING SCHEMATICS, ASSEMBLY
DRAWINGS, AND PARTS LISTS

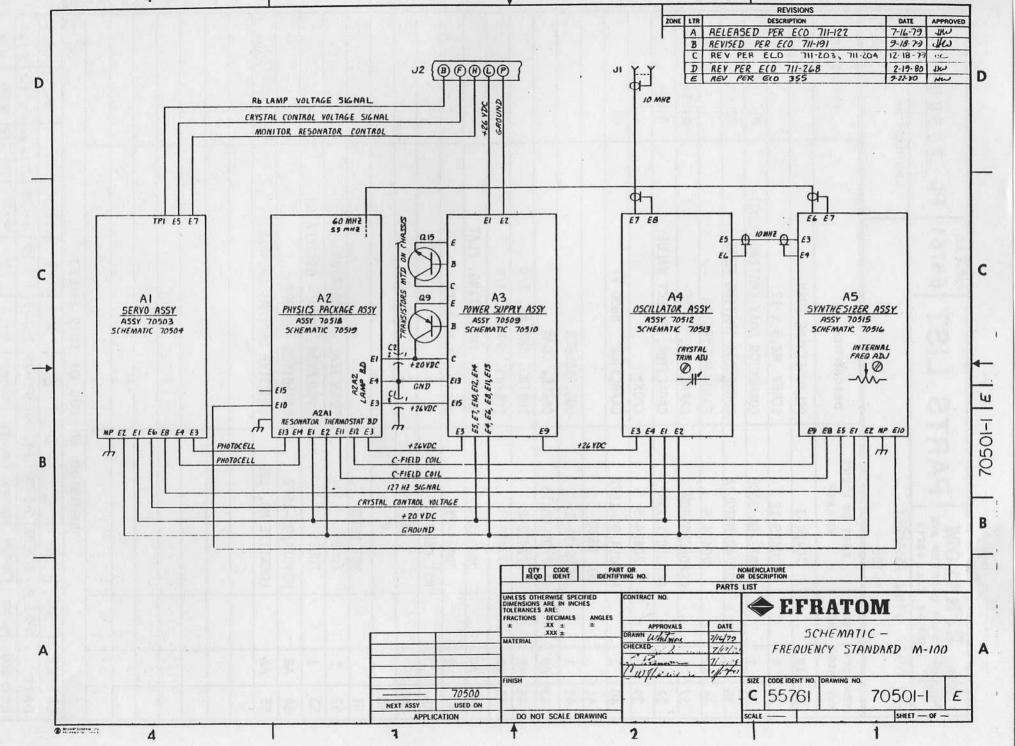
# SAMPLE TEST DATA SHEET

# MODEL M-100 RUBIDIUM FREQUENCY STANDARD

ROCEDURE	FUNCTION TESTED	NOMINAL	MEASURED VALUES		OUT OF	TOLERANCE LIMITS
STEP NO.			FIRST RUN	SECOND RUN	TOL	TOLENANGE LIMITS
(1)	(2)	(3)	(4)	(5)	(6)	(7)
				35 5		









55761

PL 70500-1

CONTRACT NO.

SHEET 3 OF 3

LIST TITLE: FINAL ASSEMBLY

M-100

6-7-79

711-107

7-5-79

711-133

5-24-79

711-67

DATE

ECO NO.

7-27-79

711-152

9-17-79

711-188

9-21-79

HW -34 ADDED -30 11-16-79

711-209 -226 12-13-79

175M 42

5.13-80 8-5-80

350

711-309

4-3-81

434

1721	15.55		M-100											3 OF 3
	QTY	FSCM NO.		OR IDEN	Т		DESCRIPT	rion					REFER	ENCE
32	AR		70424	4-3		P	OLYURET	HANE FO	AM					
33	4		70425	5-12		S	CREW M	12.5_x 12	2					
34			M39012/5			C	ONNECTO	R COAX	(MATING	PLUG)		P1		
35	William St.		M28748/8						NG PLUG)			P2		
36			70424			F	OAM, PO	LYESTER						
37	1 1000		CCR05CI6			9		R, 6.8PI				A4	C6+	
38			CCR05CXX			C	APACITO	R, SELE	CT VALUE	E		A4	C6-	3
39			70424	STATE OF THE STATE		E	POXY							
40	.1		M39014/0			C	APACITO	R 6800	0 PF			C3		
41			NOT USE											
42	1		MS35431			L	.UG, SOLI	DER						
43	AR		M 17/93-			C	CABLE, CO	OAX						
44	AR		70422					SHRINK,	1/8					
45	AR		70422			-		SHRINK,						
16	AŖ		70414-	-24		-		•	ING, FLA	AT				
47	2		70414-					E.T. L00	- 20					
48	1		NOT USED											
49				4										
50	7			-										
51			NOT US	SED	1 1		4.4							
52 :	1		70593			F	OAM SEA	L - RESC	ONATOR					
53	1		70595			I	NSULATO	R, FOAM	- OSCIL	LATOR				
54	AR		.M39014/0	)1-1572				R 6800F						
55	AR			E NO. 222	2	-			T (PURPL	E)		MIL- TYP	-S-461	163 GRADE
0														
				<u> </u>										
					- 9 - 1			· ·						
1				REVISION	N ST	ΛT	US OF	THIS S	HEFT					600411
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	En	H	D		T)			1	1 6	1	J			



6

# PARTS LIST

55761

PL 705-153-1

LIST TITLE:

SERVO ASSEMBLY

CONTRACT NO.

SHEET 2 OF 4

NO.	QTY REQD	FSCM NO.	CHAIR SERVICE	OR IDENT	DESC	RIPTION				REFER	ENCE
1	1		705	-155	PRIN	TED WIF	RING E	BOARD			
2	1		-	CGIOIJR		ACITOR				:17	
3	1			101-1353		A	560P		(	10	
9	2		M39014	101-1357			1000 P	F	0	5,07	
5	5			101-1572			800 PI	5	C	, 2, 3, 20	,21
6	1			101-1575		First L	.01 U	F		C3	0
7	-1			102-1356			.22 1	F	4	<i>-33</i>	
8	12			101-1593			.I UF	15,172,000	35-40 , 2	3, 27, 28	3,29,4
9	1			102-1419			IUF			C34	7
10	1			3/1-3006			OUF		(	4	
11	4			1/01-11425			047 UF			24, 25, 2	6,31
12	4			101-11715			IUF			13,14,15	
13	2			101-12525	CAPA	CITOR				8, (22	CAN STREET
14	3			-2207\$		STOR	220	44W		54,73	
15	+			USED	1						
16	2		RCROTG				330e	1/4 W	1	777,78	3
17	1		RCR07G			4	1,1 MEG	1/4W	./	863	
18			RCROTG			-		1/4W		37,50,51,	56,61
19	2		RCROTG				7 MEG	44 W		65,76	
20	i			2740FS			74n	1/10W		5	
21	1			14640FS			142	4	THE RESERVE AND ADDRESS OF THE PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN COLUMN TWO IS	67	
22	1			4990FS			99n		K	2	
23	1			6810F\$			812		F	16	
24	2			1001F\$			IK		R	3,49	
25	1		The second secon	2211 FS		- 2	21K			75	
26	_			USED .							78 77
27	1			3011 F\$		3.	OIK			3	
28	2			13481 FS			48K			20,66	
29	7			3571F\$			,57K			28	
30	2			19091FS			3.09 K			21,29	
31	4	TV T		1002 FS	RESI	STOR	IOK	1/0W		,60,13,	52
91			Notice of the second	REVISION :						, , ,	
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		2.H	598	6374						-	-



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# PARTS LIST

FSCM NO. 55761

PL 705-153-1

CONTRACT NO.

SHEET 3 of 4

ITEM NO.	QTY REQD	FSCM NO.	PART OR IDENT NUMBER	DES	CRIPTI	ON				REF	ERENCE
32	1		RNC55H1502F\$	RES	ISTOR	15K				R4	
33	1		RNCSSH 1872 FS		4	18.71	r			RI	
34	1		RNC55H2743FS			274				R62	
35	i		RNC55H2742F\$			27.41				R48	
36	2		RNC55H 3322 FS			33,2 K				R17, F	246
37	1		RNC55H3922F\$			39.2 K	٤			R47	-
38	T		RNC55H 4752F\$			47.5K		Reserved to		R42	
39	1		RNC55H 5622F\$			56.2k	<b>C</b> (1)	9 45m	heri,		COLUMN TO SECURIT DE LA VALOR DE LA COLUMN D
40	3		RNC55H 8252F5			82,51	K			R27,5	
41	10		RN(55H1003F\$			IOOK	L A	7,9,11,2	5,32,	38,43,	79,44,8
	-		Kittasiii		1	YOT U					
42	1		RNC55H3323FS			332K	4			R55	
44	1		RNC55H4223FS			4221				R35	
45	1		RNC55H1004 FS			IME	G			R 5	9
46	,		RNC55H2004F5		-	2me				RIZ	
47	-		RNC55H XXXX FS	RE	515701	e, SEL		ALVE		R19,22	23,30,36
48	5		RWR80\$1000FS		STOR		L 2V			R68	
49	1		NOT USED								
50	-		NOT USED								
51	1		JANTX IN 4153	DI	ODE					:	_ CR9
52	2		M575084-4			OR 2	2UH			11,2	
53	-		NOT USED	1							
	1	*	JANTX 2 N 3501	TR	ANSI!	STOR				QI	
54	1	1	M38510-10703BXC			REG				VRI,	VRZ
55	2		70495-1	IN	TEGR	ATED	CKT	883/40	53 BC)		
56	,		70496-1	110	1		(MA	725HMQ	B)	UI	
57	1		NOT USED			-	,				
58	<u>-</u>		NOT USED								
59	1-				-					U5	
60	+		M38510-10104 BGX		-		(LMI	145/883	3)	16,0	12
61	2		M38510-11005 BCX	IN	TEGI	PATED	_			U3	
62	1		REVISION								
		1 4			E.	F		T			
-	TTER	A				and the second second					
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LIST TITLE:

# PARTS LIST

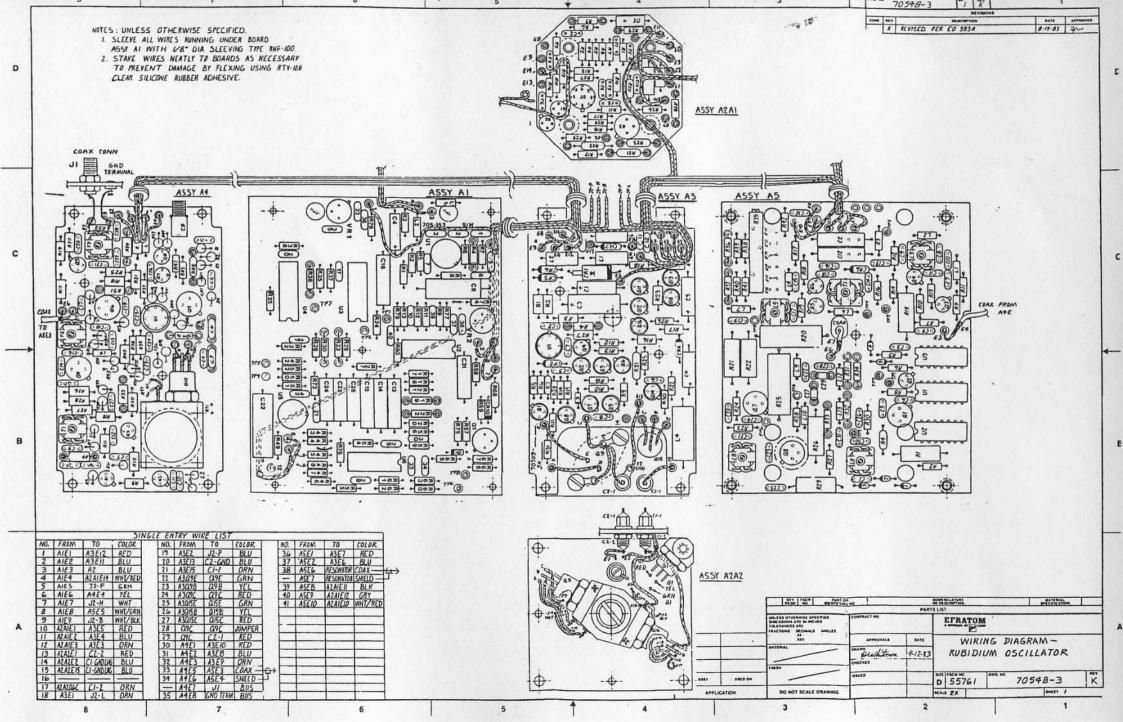
FSCM NO. 55761

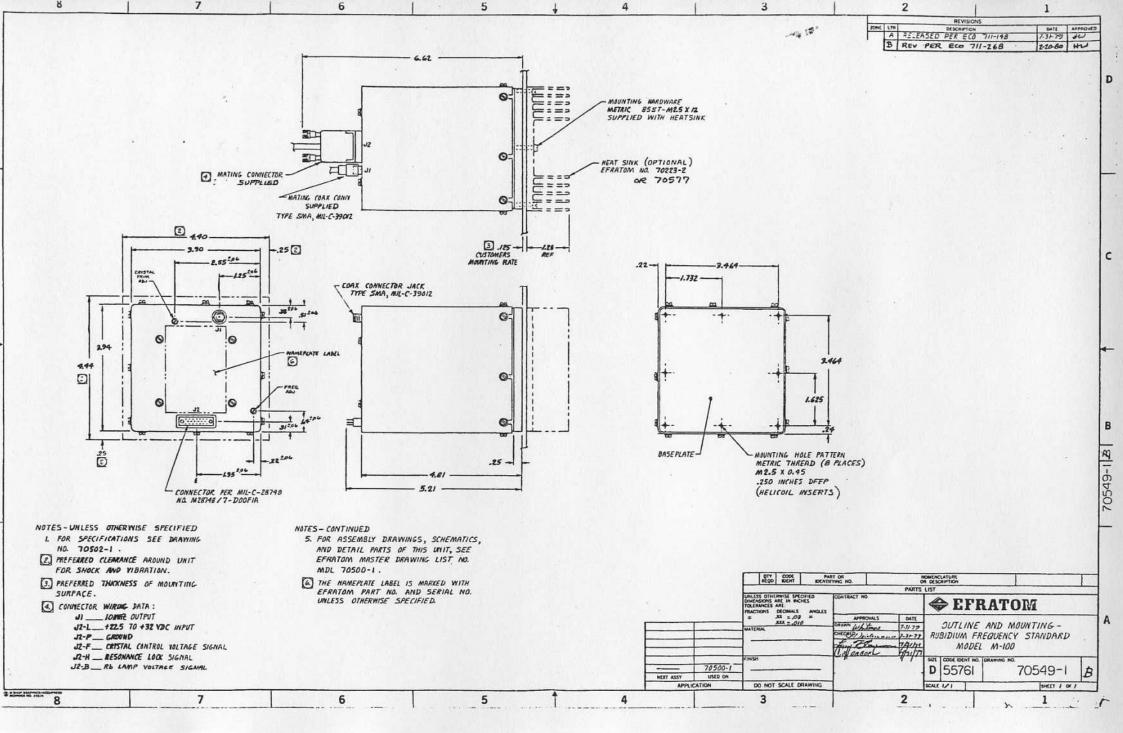
PL 705-153-1

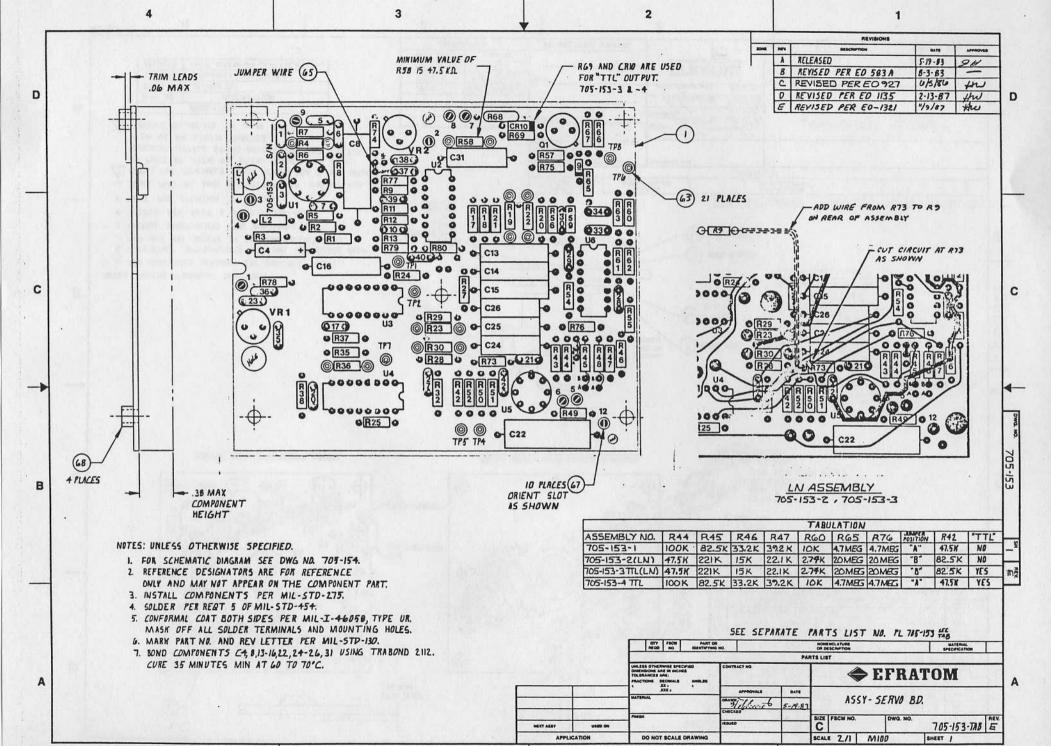
CONTRACT NO.

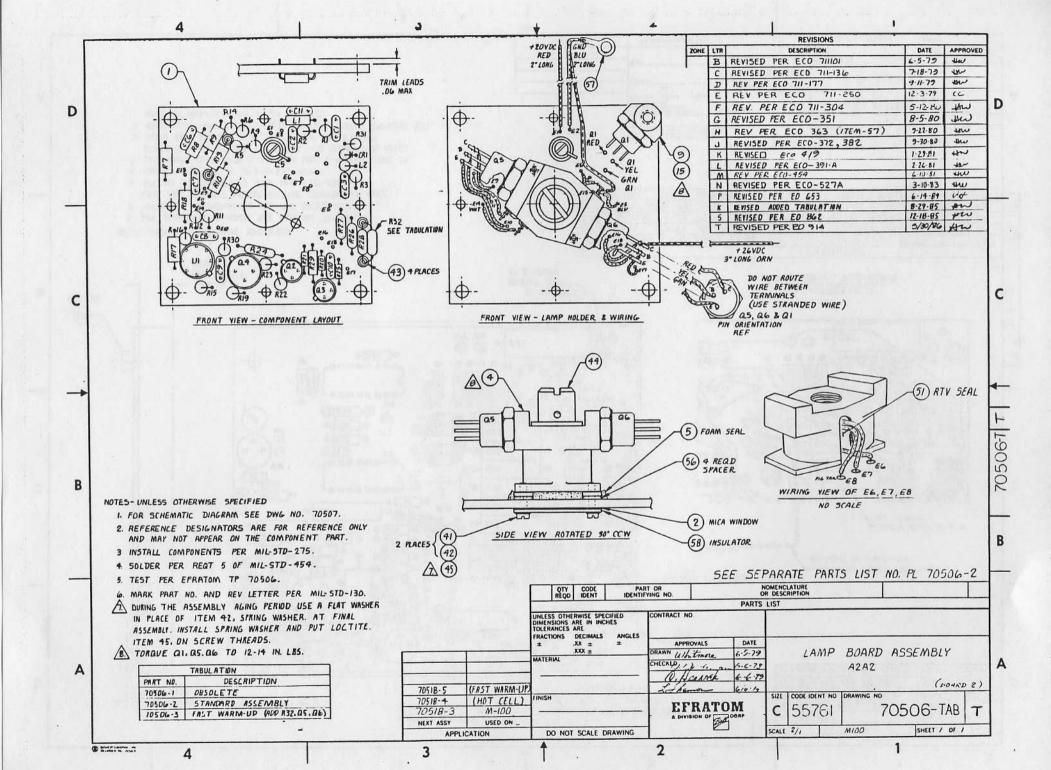
40F\$

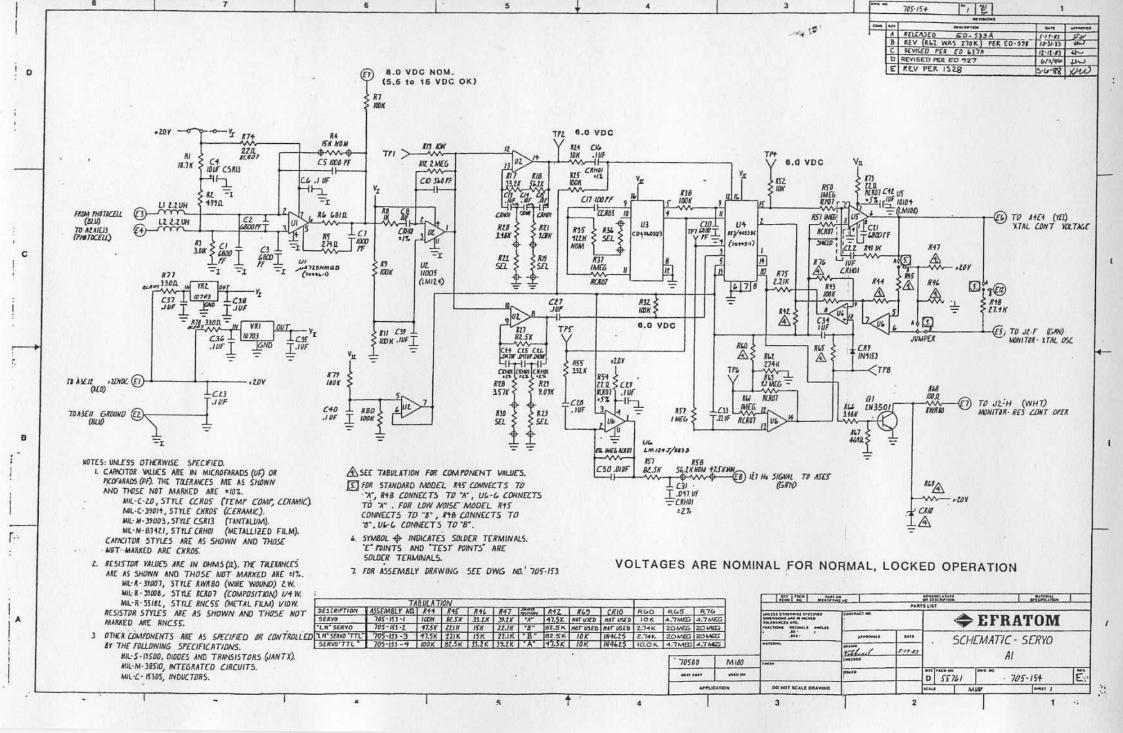
NO.	QTY	FSCM NO.	PART OR IDENT NUMBER	DESCRIPTION	REFI	ERENCE
63	21		SE16XCOZ	TERMINAL -TURRET		
64	3		70418-1	MOUNTING PAD	XQIX	YRI, XVR
65	AR		QQ-W-343.TYPE S	WIRE, TINNED COPPER 24AWG		
66	2		M38527/4-03N	MOUNTING PAD	XUI,	XU5
67	10	Finit	70416-3	TERMINAL, BIFURCATED		
68	4		70417-1	STANDOFF - PEM		
69	i		RNC 55H68I2FS	RESISTOR 68.1 K	R58	
	Are		205 164	SCHEMATIC		
-	REF		705-154	SCHEMATIC		
				The state of the s		
			WAR AND			
			State 6			
			S COUNTY OF STREET			
				HEN JANTX2N3501 IS NOT AVAILABLE, SE JANTX2N5662 OR 704-262 AS AN		
				CCEPTABLE ALTERNATE.		
	374		TO CONTRACT OF THE PARTY OF THE			
			REVISION S	TATUS OF THIS SHEET		
LE.	TTER	TA	RCT	) E		
DA	TE	5.20	1-83 2-13-87 1-11-88 4-13	-88 5-4-88		

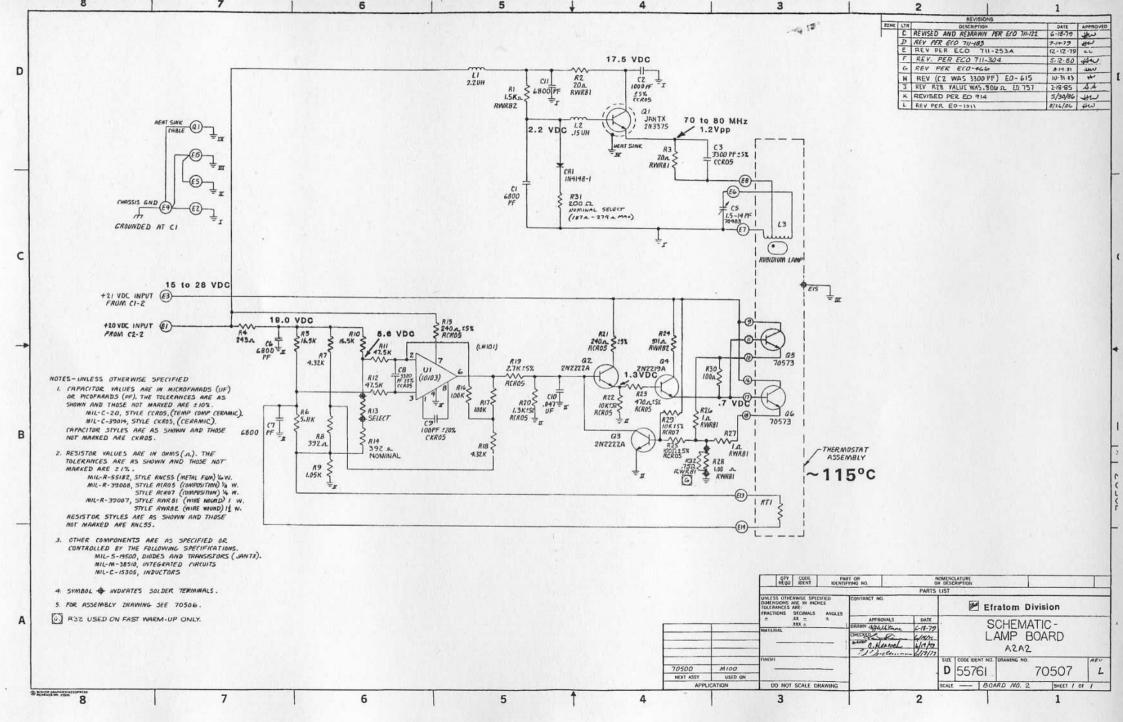














55761

PL 70506-2

LIST TITLE:

LAMP BOARD ASSEMBLY

CONTRACT NO.

SHEET 2 OF 3

25550, 12.00	QTY REQD	FSCM NO.	PART OR IDENT NUMBER	DESCRIPTION	REFERENCE
1	1		70508	PRINTED WIRING BOARD	
2	1		70596	WINDOW, MICA	
3	_	MOTOPALA	705-142	TRANSISTOR, CUT OFF (JANTX2N3375)	01
4	1		70576	THERMOSTAT ASSEMBLY	
5	1		70597	SEAL, FOAM	
6	2		CCRO5CG332JR	CAPACITOR 3300PF, 50V	C3,C8
7	1		M39014/01-1340	CAPACITOR 100PF	C9
8	4		M39014/01-1572	CAPCITOR 6800PF	C1,6,7,11
9	1		705-141	POST, TRANSISTOR MOUNT	
10	1		M39014/01-1587	CAPACITOR, .047UF	C10
11	1		70403	CAPACITOR, VARIABLE, 1.5-14PF	C5
12	1		JANTXIN4148-1	DIODE	CRI
13			70412-2	INDUCTOR 2.2UH (MS75084-4)	Ll
14	1		70412-1	INDUCTOR .15UH (MS75083-3)	L2
15	1		70425-15	SCREW, METRIC, M3x6	
16			UANTX2N2222A	TRANSISTOR	Q2,3
17			JANTX2N2219A	TRANSISTOR	Q4
18			RNC55H1000FS	RESISTOR 100 n 1/10W	R30
19			RNC55H2430FS	RESISTOR 243 \$\Omega\$1/10W	R4
20			RNC55H3920FS	RESISTOR 392 1/10W (R14, NOMINAL	R8,14
21	1		RNC55H1051FS	RESISTOR 1.05KA 1/10W	R9
22	1		RNC55H4321FS	RESISTOR 4.32KR 1/10W	R7,18
23			RNC55H5111FS	RESISTOR 5.11KA 1/10W	R6
24	+		RNC55H1652FS	RESISTOR 16.5K% 1/10W	R5,10
11			RNC55H4752FS	RESISTOR 47.5K \$\mathcal{X}\$ 1/10W	R11,12
25			RNC55H1003FS	RESISTOR 100K A 1/10W	R16,17
	2		RNC55HXXXXFS	RESISTOR SELECT 1/10W	R13
27			RCRO5G101JS	RESISTOR 100 A 1/8W	R25
28			RCRO5G241JS	RESISTOR 240 A 1/8W	R15,21
29		1 3 5	RCRO5G241JS	RESISTOR 470 & 1/8W	R23
30			RCRO5G132JS	RESISTOR 1.3K 2 1/8W	R20
31	1 1			STATUS OF THIS SHEET	
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-	CO N				



FSCM NO.

55761

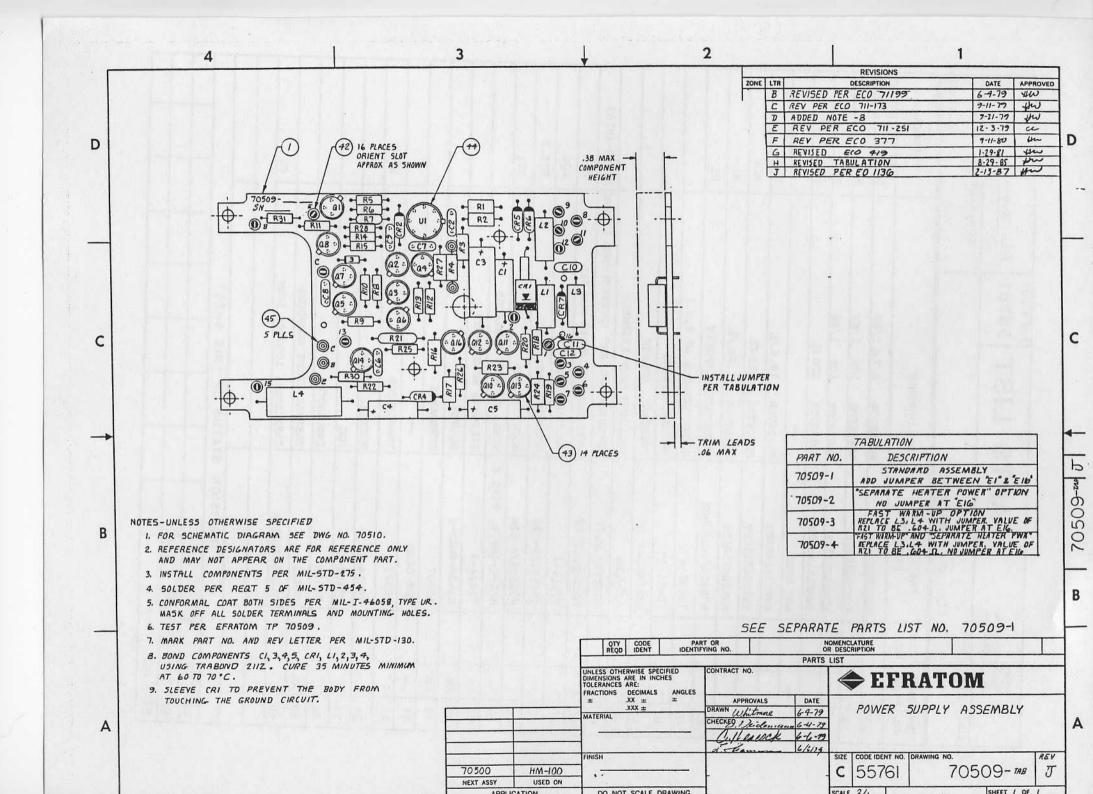
PL 70506-2

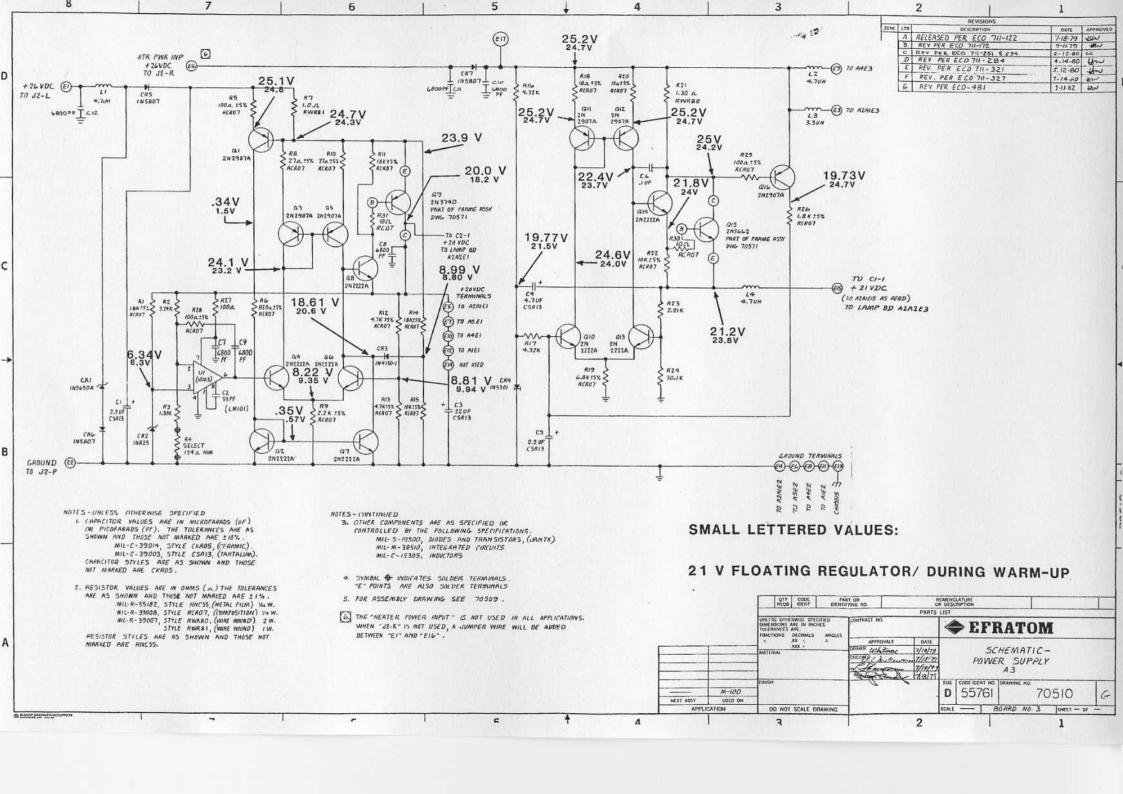
LIST TITLE:

DATE ECO NO. CONTRACT NO.

SHEET

3 OF 3 LAMP BOARD ASSEMBLY REFERENCE PART OR IDENT DESCRIPTION QTY FSCM ITEM NUMBER NO. REQD NO. R19 2.7 1/8W RESISTOR RCRO5G272JS 32 R22 10K 1/8W RESISTOR RCRO5G103JS 33 R29 10K 1/4W RESISTOR RCRO7G103JS R26,27,28 34 100 2 RESISTOR RWR81S1RooFS 3 35 NOT USED 36 R2,3 19.6元 RESISTOR RWR81S19R6FS 2 37 R24 511 5 RESISTOR RWR80S5110FS 1 38 R1 1.5K 12 RESISTOR RWR80S1501FS 1 39 U1 INTEGRATED CIRCUIT M38510/10103BGX 1 40 SCREW (M2x8mm LG S.S.) 70425-4 2 41 WASHER, SPRING 70414-19 2 42 TERMINAL, SOLDER SE16XC02 43 4 RUBIDIUM LAMP ASSEMBLY 705-110 ADHESIVE SEALANT (PURPLE) TYPE II GRM MIL-S-46163 44 1 LOCTITE #222 45 AR R31 RESISTOR, 200 1%W NOM SEL RNC55H2000FS 1 46 XQ4 MOUNTING PAD 70418-1 47 1 XQ2,3 MOUNTING PAD M38527/3-02N 2 48 XU1 MOUNTING PAD M38527/4-03N 49 1 WIRE, 24 AWG, STRANDED MIL-W-16878 TYPE E 50 AR SILICONE RUBBER-RTV 70424-7 51 AR SOLDER SN63W-RMAP-3 AR 52 SCHEMATIC 70507 53 REF NOT USED 54 05,6 TRANSISTOR 70573 55 2 WASHER, FIBER 70414-1 56 4 LUG 70421-1 57 1 INSULATOR 70559 58 1 THERMAL JOINT COMPOUND 70411 59 AR C2 CAPACITOR, 1000PF, 100V CCR05CG102JR 1 60 STATUS OF THIS SHEET REVISION LETTER 0/26/36







FSCM NO. 55761

PL 70509-1

LIST TITLE: POWER SUPPLY ASSY A3

CONTRACT NO.

SHEET 2 of 3

ITEM NO.		FSCM NO.		OR IDEN	Г	DESCRIPT	rion				REFE	RENCE
1	1		705	511		PRINTED	WIRING	BOARD				
2	1		M39014/0	11-1330		CAPACITO	R	33PF	TE WATER		C2	
3	6		M39014/0			4	681	00PF			C7, 18, 9,	10,11,1
4	1		M39014/0					.1UF			C6	
5	2		M39003/0				2	.2UF			C1,C5	
6	1		M39003/0	1-2848		Y	4	.7UF			C4	
7	1		M39003/0	1-3026		CAPACITO	R 1	22UF			C3	
8	1		70428			DIODE	(IN56	550A)	- 62 - 53		CR1	
9	1		JANTX1N8	25		4					CR2	
10	1		JANTX1N4	150-1							CR3	
11	1		JANTX1N5	5301		4			₩		CR4	
12	3		JANTX1N5			DIODE					CR5-7	
13	2		MS7510			INDUCTOR	₹ 4	.7UH (N	MS75101-	3)	L1,L2	
14	1		MS7510		The same of the same of	INDUCTOR		11111	MS75101-		L3	
15	1		M59118			INDUCTOR			MS91189-	C	L4	
16	8		JANTX2N2		II COMMENTED TO THE PARTY OF TH	TRANSIST		4-5		02,		10,13,1
17	6		JANTX2N2			TRANSIST					Q1,3,5,11	
18				ΓUSED								
19				Γ USED								
20				T USED								
21	1		RNC55H10			RESISTOR	1	00Ω			R27	
22	1		RNC55H15			4			NOMINAL)		R4	
23	1		RNC55H13				1.30				R3	
24	4			USED		4					1	Fed little
25	1		RNC55H32			RESISTOR	3.24	4ΚΩ			R2	
26	2		RNC55H43			RESISTOR					R16,17	
27	1		RNC55H22	San		1	2.2				R23	
28	1		RNC55H30				30.11				R24	
29	4		RCR07G10					0Ω			R18,20,	30.31
30	2		RCR07G27		IV IV	.7		7Ω			R8,10	
31	3		RCR07G10			RESISTOR					R5,25,28	
31	31					TUS OF		NEW YORK				
LETT	ΓER	E	F	G	Н	TJ	K	L				T
DATI	110.00	7-18-79	397			7-14-80		- F	37			
	NO.	N/C			711-271		481	1393				



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PL 70509-1

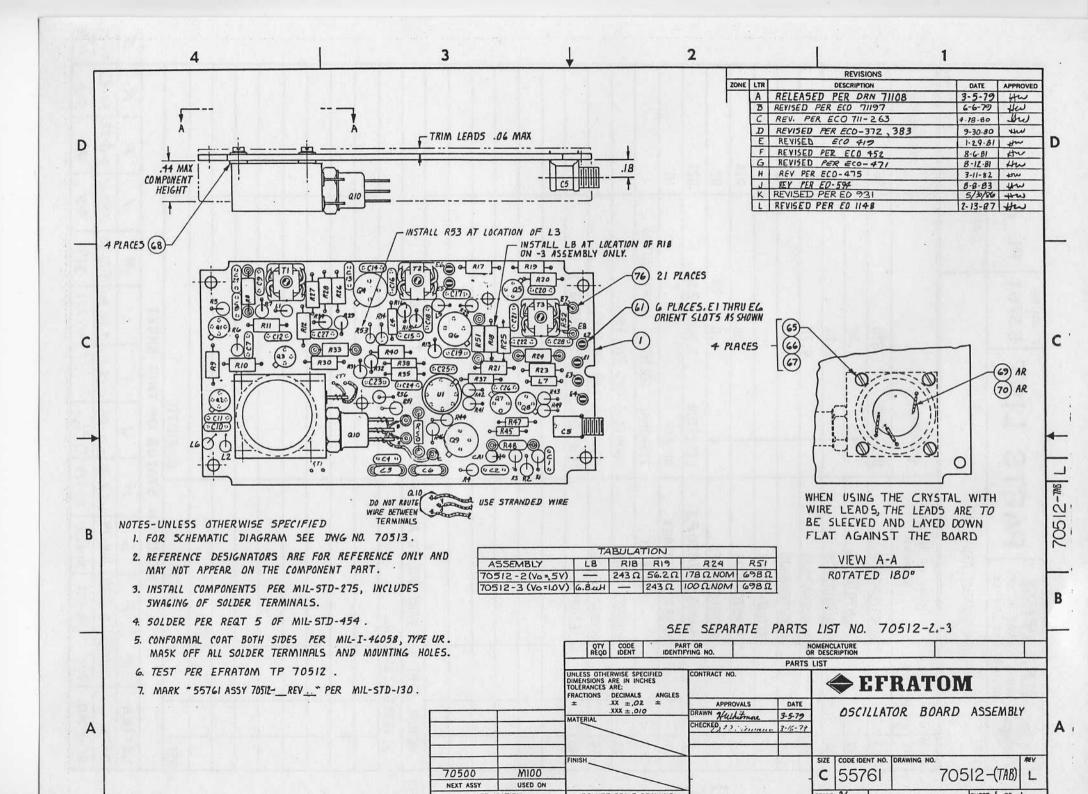
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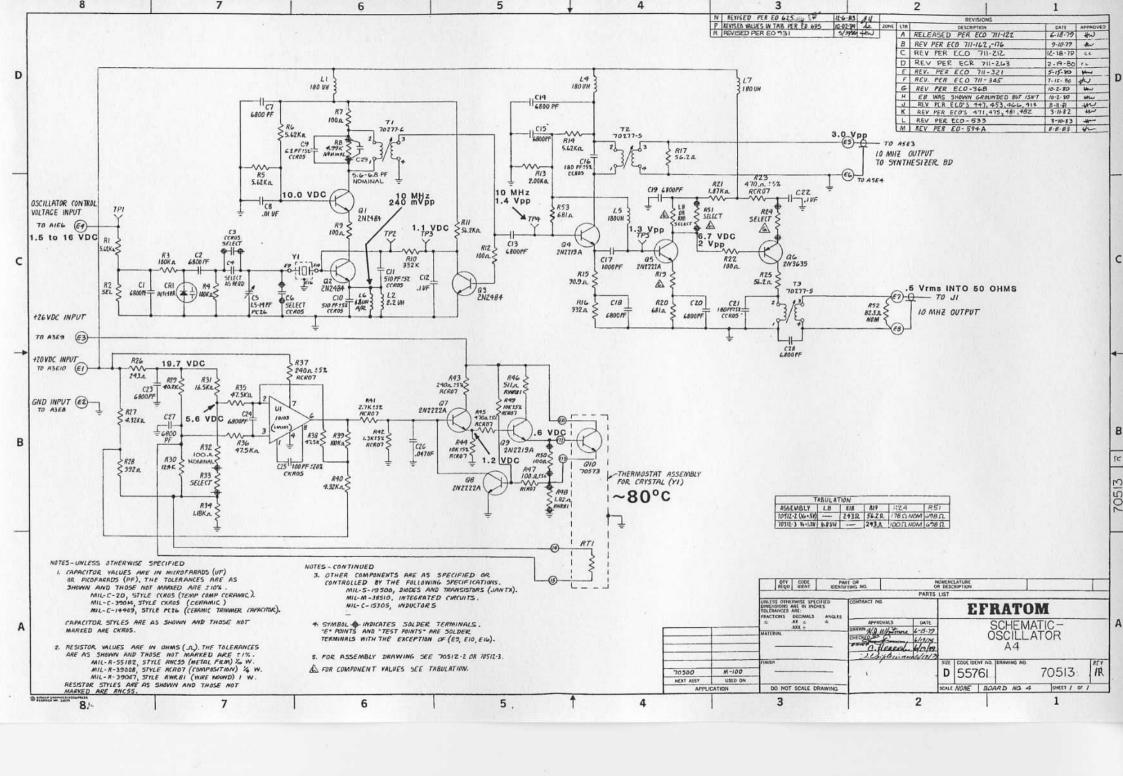
POWER SUPPLY ASSY A3

CONTRACT NO.

3 of 3

												3 OF 3
TEM NO.	QTY REQD	FSCM NO.		OR IDENT	ī	DESCRIPT	ION				REFERE	NCE
32	1		RCR07G82	1JS	R	ESISTOR	{	320		R	6	
33	2		RCR07G18	2JS			1.	.8K		R	26, R1	
34	1		RCR07G22	2JS			2.	2K		R	9	
35	2		RCR07G47	2JS		*	4.	.7K		R	12,13	
36	1		RCR07G682	2JS			6.	.8K		R	19	
37	3		RCR07G103	3JS			•	l O K		R	11,15,22	
38	1		RCR07G18	3JS				18K		R	14	
39	1		RWR81S1R	00FS		1		1.0 1	W	R	7	
40	1		RWR80.5		S F	RESISTOR	1.	300.2	W	R	21	
41	1		M38510/1			P AMP			TA, La	U	1	
42	16:			16 _3		ERMINAL	, SOLDE	R (BIF	URCATED)	)		
43	14		M38527/3			OUNTING						
44	1		M38527/4			OUNTING						
45	5		SE16XC02			ERMINAL			T)			
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DAT		7-18-79		11-16-79		2-12-80				1-29-31		
ECC	NO.	N/C	711-173	711-229	711-259	711-251	711.234	7/1-327	347	419	481	513







55761

PL 70512-1

CONTRACT NO.

SHEET 2 OF 4

OSCILLATOR BOARD ASSEMBLY (A4)

NO.	REQD	FSCM NO.		OR IDEN	Т	DESCRIP	TION				REFE	RENCE
1	1		705	14		PRINTED	WIRING	BOARD				
2	1		705	72		CRYSTAL	THERMOS	TAT ASS	1			
3	1		CCR05C	J5R6D	R	CAPACIT	OR 5	GPF	Nomine	<del>1</del> ک	C29	
4	1		CCR05CG6	20JR		CAPACITO	R 6	2PF			C9	
5	2		CCR05CG1	81JR		1	18	OPF			C16,C21	
6	2		CCR05CG5	11JR			51	OPF			C11,C10	
7	-		NOT	USED								
8	3		CCR05CGX	XXJR			SE	LECT VAL	LUE		C3,C6,C4	1
9	1		M39014/0	1-1340			10	OPF			C25	
10	1		M39014/0	1-1357			100	OPF			C17	
11	13		M39014/0	1-1572			680	OPF		C1,2,	7,13,14,	15,18,1
-			•——			-			- 1		20,23,24	,27,28
12	1		M39014/0	1-1575			.0	1UF			C8	
13	1		M39014/0	1-1587			.0	47UF			C26	
14	2		M39014/0	1-1593		CAPACITO	R .1	UF			C12,C22	
15	1		PC26J140			CAPACITO	R, VAIR	ABLE 1-	14PF		C5	
16	1		JANTXII	151481	A	DIODE, V	ARACTOR	(7.11.21.	٠,		CR1	#
17	1		M\$750	84-4		INDUCTOR			75084-4	)	L2	
18	1		704	12-3		INDUCTOR	3.	9UH (MS	75084-7	)	L3	
19	1		MS7508			INDUCTOR	- William - O O.		75084-10	21/21	L6	
20	4		M575Q8	35-10		INDUCTOR			75085-10		L1,4,5,	7
21	3		JANTX 2N			TRANSIST	The control of the same				Q1,2,3	
22			JANTX2N2			TRANSIST					Q9	
23	5		JANTX2N2			TRANSIST					Q4,5,7,	8
24	1		JANTX2N3	635		TRANSIST	OR				Q6	
25	1		RNC55H47	R5FS		RESISTOR	47.5	Ω			R18	
26	3		RNC55H56	24 10 10 10 10 10 10 10 10 10 10 10 10 10	1 1	4	56.2				R17,19,	25
27	2		RNC55H90				90.9		·· Nomi	441	R15, R5	
28	6		RNC55H10				100		Nomi		R32,7,9,	
29	1		RNC55H24				243	- triber	- NOME		R26	
30	1		RNC55H33			RESISTOR					R16	
				EVISIO	N STA	TUS OF						
ET	TER	A	B	С	D	E	F	G	H	J	K	
TAC	E	5-24-79	7 6-5-79	7-10-79	9-10-7	9 10-31-79	2-19-80	9-22-80	6-11-81	5-13-8		7
ECO	NO.	711-64	711-103	711-141	711-162	- 711-212	711-263		Eco-453	1234		



OSCILLATOR BOARD ASSEMBLY (A4)

FSCM NO. 55761

PL 70512-1

CONTRACT NO.

711.259

711-250

711-263

711-345

383

SHEET 3 of 4

ITEM QTY FSCM PART OR IDENT DESCRIPTION REFERENCE REQD NO. NO. NUMBER R28 392Ω 31 RNC55H3920FS RESISTOR 1 475Ω R23 32 RNC55H4750FS 1 681Ω R20 33 1 RNC55H6810FS 34 NOT USED NOT USED 35 R34 36 1 1.18ΚΩ RNC55H1181FS R21 37 1 RNC55H1871FS 1.87ΚΩ R13 38 RNC55H2001FS 2.00ΚΩ 1 39 2 RNC55H4321FS 4.32KΩ R27,40 40 4 RNC55H5621FS 5.62KΩ R1,5,6,14 41 1 RNC55H1242FS 12.4KΩ R30 42 1 RNC55H1652FS 16.5KΩ R31 1 43 RNC55H4022FS 40.2KΩ R29 44 3 RNC55H4752FS 47.5KΩ R35, R36, 38 45 1 RNC55H5622FS 56.2KΩ R11 100ΚΩ 46 3 RNC55H1003FS R3,4,39 47 2 RNC55HXXXXFS SELECT VALUE R2, ,33, 1 48 RCR07G101JS  $100\Omega$ R47 49 RCR07G241JS 240Ω R37,43 50 1 RCR07G471JS 470Ω R45 51 RCR07G132JS  $1.3K\Omega$ R42 52 1 RCR07G272JS 2.7KΩ R41 53 2 RCR07G103JS 10ΚΩ R44.49 1 54 RNC55H3323FS 332KΩ R10 55 1 RNC55H4991FS 499K NOMINAL R8 56 1 RWR81S1R82FS  $1.82\Omega$ 1W **R48** 57 1 RWR81S5110FS RESISTOR 511Ω 1W R46 58 2 70406-5 TRANSFORMER (RED-GRN-BLU-WHT) T2, T3 59 1 70406-6 TRANSFORMER (GRN-RED-WHT-YEL) TI 60 1 M38510/10103BGX INTEGRATED CIRCUIT, OP-AMP U1 6 61 TERMINAL, SOLDER (BIFURCATED) 70416-3 REVISION STATUS OF THIS SHEET C B D LETTER A E F 0 H J L K 5-24-79 6-5-79 9-26-79 10-31-79 11-16-79 DATE 9-10-79 1-28-80 2-19-80 1.18.80 7-15-80 10-1-80 711-176 711-199 711-212 ECO NO. 711-64 711-230 711-103

711-213

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FSCM NO.

PL 70512-1

LIST TITLE: OSCILLATOR BOARD ASSEMBLY (A4) CONTRACT NO. SHEET 4 of 4 ITEM QTY FSCM PART OR IDENT DESCRIPTION REFERENCE NO. REOD NO. NUMBER XQ6,9 MOUNTING PAD (TO-5) 70418-1 62 2 XQ1-5,7,8 MOUNTING PAD (TO-18) 7 M38527/3-02N 63 MOUNTING PAD (8-PIN) XU1 1 M38527/4-03N 64 65 4 70425-3 SCREW WASHER, SPRING 4 70414-18 66 WASHER, FLAT 67 4 70414-4 70414-1 WASHER, FIBER 68 4 WIRE, TINNED COPPER, 30 AWG QQ-w-343, TYPE S 69 AR SLEEVING, TEFLON, 30 AWG MIL-I-22129 70 | AR 71 AR SN63WRMAP3 SOLDER POLYURETHANE, CONFORMAL COAT MIL-I-46058, TYPE UR 72 AR SCHEMATIC DIAGRAM 70513 73 REF TP 70512 TEST PROCEDURE 74 REF 75 AR MIL- W-16878, TYPE E WIRE, STRANDED, 30 AWG, TEFLON SOLDER TERMINAL (TURRET) 76 21 SE16XCOZ R24 . 77 1 RESISTOR 101 NominAL RNC55HIORO RNC55HB2R5FS RESISTOR 82.5 IL NOMINAL R52 78 - 1

AC	TUAL	PART	MAY VARY	DUE TO	AVAILABILITY, SEE	ECO 711-250	FOR
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711-230

LETTER

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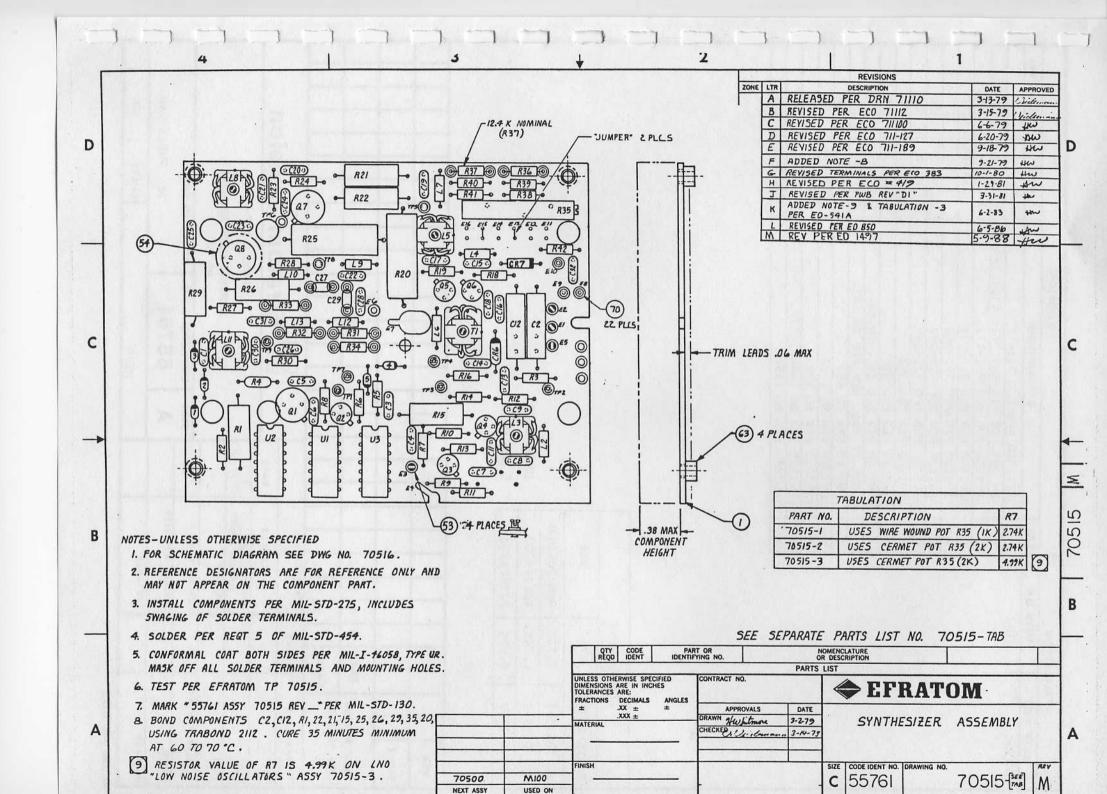
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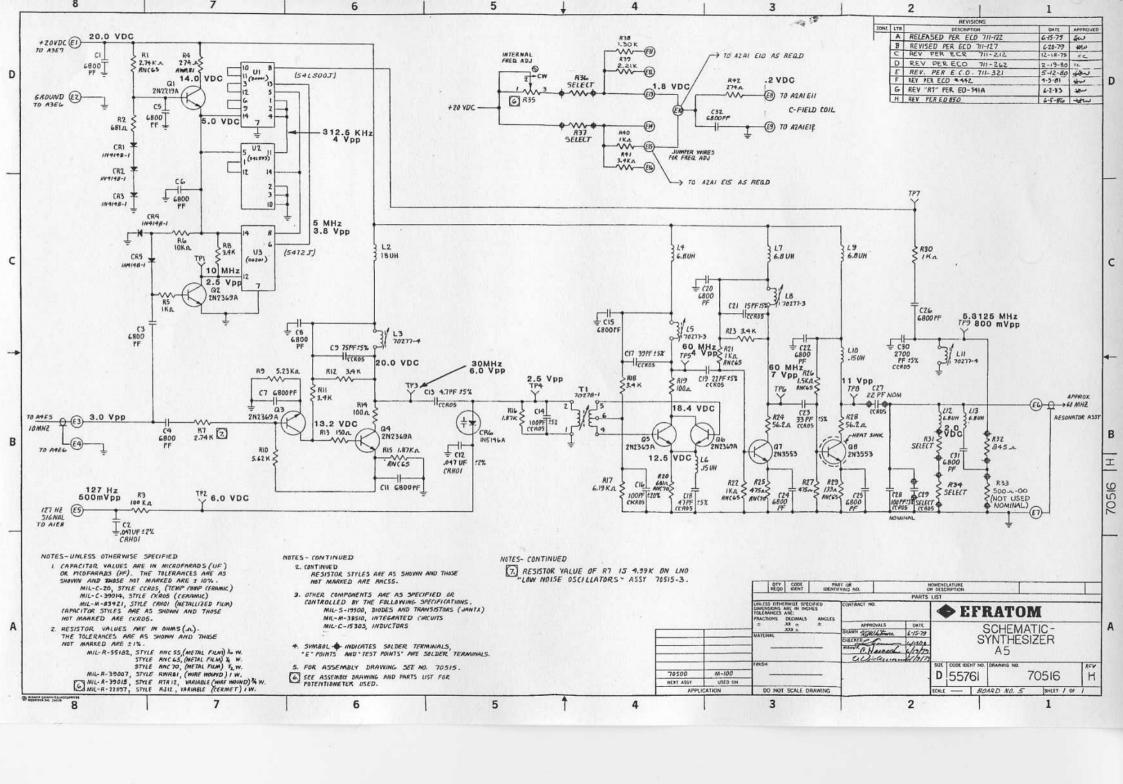
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1-29.81 12-6-83 2-13-87

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55761

PL 70515 -: 13

LIST TITLE:

SYNTHESIZER ASSEMBLY

CONTRACT NO.

SHEET 2 OF 4

NO.	QTY REQD	FSCM NO.		OR IDEN	Τ	DESCRIP	TION				REFERENCE
1	1		70!	517		PRINTED	WIRING	BOARD			EFRATOM
2	1		CCR050	G4R7DF		CAPACITO	R 4.	7PF			C13
3			NOT	USED		A					
4	1		CCR05CH	150JR			1	5PF		,	C21
5	2/		CCR05CG2	220JR			2	2PF (C2	7 NOMIN	AL)	C19, C27
6	1		CCR05CG	330JR			3	3PF			C23
7	1		CCR05CG	390JR			3	9PF			C17
8	1		CCR05CG4	470JR			4	7PF			C18
9	1		CCRO5CG	750JR			7	5PF			C9
10	2		CCR05CG	101JR			10	OPF (C2	8 NOMIN	AL)	C14,C28
11	1		CCR05CG	XXXJR			SE	LECT (47	-120PF)	male	, C29
12	1		CCR05CG	272JR	093	CAPACITOR	7 270	OPF			C30
13			· NOT US	5ED							
14	17		M39014/0	01-1572		CAPACITO	R 680	OPF			C1,C3-8,11,15
_									C32,	20,22	,24,25,26,31
15	2		M83421/0	01-11425		CAPACITO	R .04	7UF			C2,C12
16	6		JANTX1N4			DIODE					CR1-CR5,CR7
17	1		JANTX1N		ž	DIODE, V	ARACTOR		2.000		CR6
18	2		M\$ 750	83-3		INDUCTOR	.1	5UH (MS7	5083-3)		L6,L10
19		an I	NOT	USED							
20	5		MS75	084-10		INDUCTOR	6.	8UH (MS7	5084-10	)	L4,7,9,12,13
21	1		M5750	184-15		INDUCTOR	1.	8UH (MS7	5084-15	)	L2
22	2		704	106-3		INDUCTOR	VARIAB	LE (RED-	YEL)		L5,L8
23	2		704	106-4		INDUCTOR					L3,L11
24	1		JANTX2N2	2219A	4	TRANSIST	OR				Q1
25	3		JANTX2N2			TRANSIST	OR				Q2-4
26	2	60.4	JANTX2N3	3553		TRANSIST	OR				Q7-8
27	4		RNC55H56			RESISTOR		56.2Ω			R24,28,19,20
28	1		RNC55H1			RESISTOR		100Ω			R14
29	1		RNC55H1			RESISTOR		150Ω			R13
30	1		RNC55H47	- Interest		RESISTOR		475Ω			R27
301				REVISIO	N ST	ATUS OF					
LET	TER	A	B	C	D	E	F	G	Н	J	
DAT	E	6-20-	19 9-10-79	+	8-17-8		5-13-87	12-7-87		A 100 A 100 A	38
ECO	NO.	711-127	711-193	711-262	Eco-44	2 850	1234	1393	1497	155	



FSCM NO. 55761

PL 70515-748

CONTRACT NO.

SHEET 3 of 4

LIST TITLE: SYNTHESIZER ASSEMBLY

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ITEM NO.	QTY REQD	FSCM NO.	V 2000 2000 1000 1000 1000 1000 1000 100	OR IDENT		DESCRIPTI	ION	KINEW TO				REFEREN	ICE
31	1		RNC55H68	IOFS		RESISTOR	681	Ω			R2		
32	3		RNC55H100	1FS		4	1 K	ດ			R5,	40,30	)
33	1		RNC55H187	1FS			1.87K	Ω			R16		
34	5		RNC55H340	1FS			3.4K	Ω		R8,	11,	12, 2	23,41
35	1		RNC55H523	B1FS		•	5.23K	Ω	A RIDELL		R9		
36	1		RNC55H562	21FS		RESISTOR	5.62K	Ω	Berlandon.		R10	)	
37			NOT US	ED					i de la la				
38	7		RNC55H100	D2FS		RESISTOR	7 10K	Ω			R6,	18	
39	1		RNC55H100	O3FS		<b>A</b>	100K	Ω			R3		
40	4		RNC55HXXX	KXFS			SELE	CT (100s	2-12ΚΩ)		R31	,-34,37	,33
41	1		RNC65H133	30FS			133Ω				R29	)	
42	2		RNC65H100				1 K	Ω	TO THE THINK		R21	,22	
43	1		RNC65H150				1.5K	Ω			R26	5	
44	1		RNC65H18				1.87K	Ω.			R15	5	
45	1		RNC65H274			V	2.74K	Ω.			R1		
46	1		RNC70H47			RESISTO	R 475	Ω			R25	5	
47			NOT US						MANUAL	WI L			
48	1		RWR81S27			RESISTOR	274	Ω			R4		
49	1			06-7		TRANSFORM		PIN)			T1		Mari
50	1		M38510/	A STATE OF THE PARTY OF	C.X	INTEGRATI		IIT			U1		
51	1		M38510/			INTEGRATI	THE RESERVE TO SERVE				U2		
52			M38510/			INTEGRA					U3		
53	4			163	181	TERMINAL		2010	JRCATED)				
54				201	3181	HEAT SIN						211	
55				18-1	1,01	MOUNTING		)-5)		14	XQ	1,7,6	
56	C 1 - 310		M38527/3	Carrier and		MOUNTING					XQ	2-6	
			SN63WRMA			SOLDER					QQ	-S-571	M.I
57	AR	TE GE	705			WASHER, M'	YI AR		. 2	eu.	XQ8	8	
58			ZXTUAZ	The second secon	4	TRANSIS	STATUTE THE					0.00	
59			MIL-I-46			POLYURET		ONFORMAL	COAT)				
60	AR		RNC55H27		L OIL	RESISTOR					R4	2	
61				REVISIO	N ST	ATUS OF	e carrie	200					
157	TER	1 1	$\mathcal{B}$	C	D	E	F	G	Н	J	T	K	L
DAT	TER	A		926-79	11-16-79		2-19-80				-81	8-10-81	6-2-83
	O NO.	6-20-		711-199	711-231			7/1-269		411-	-	461	54/A
200	J NO.	11-12	7 711-189	111773	1111-231	74, 500				,,,,		460	



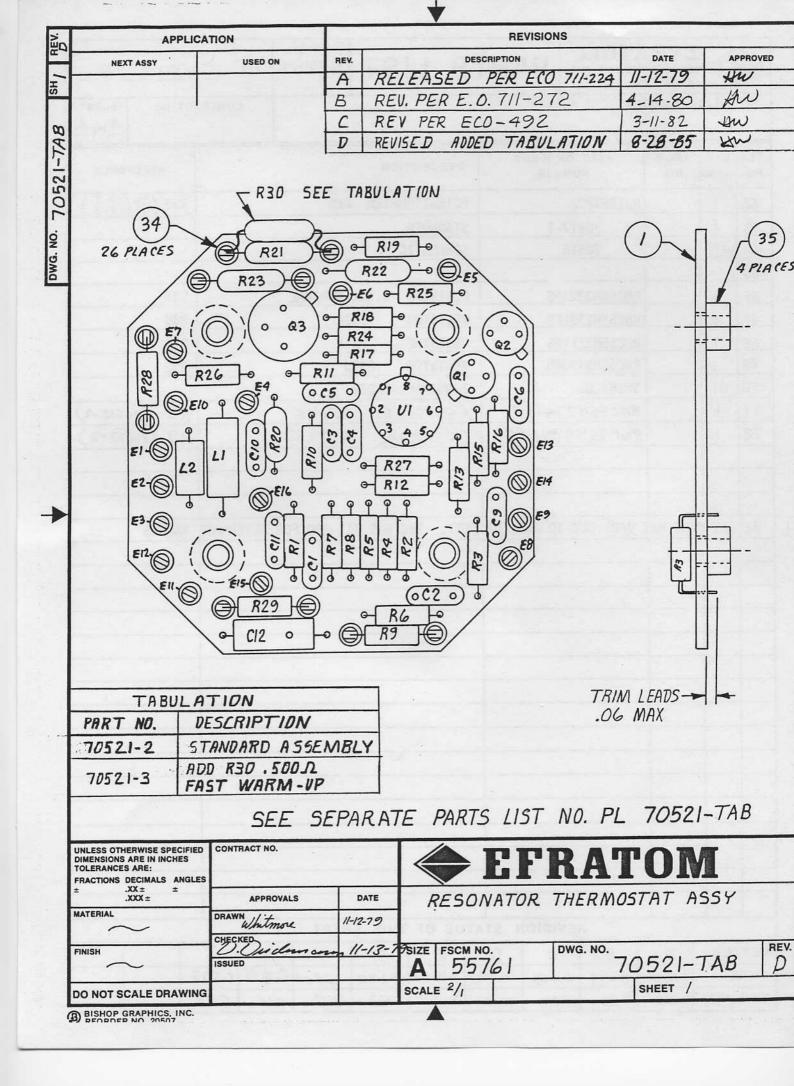
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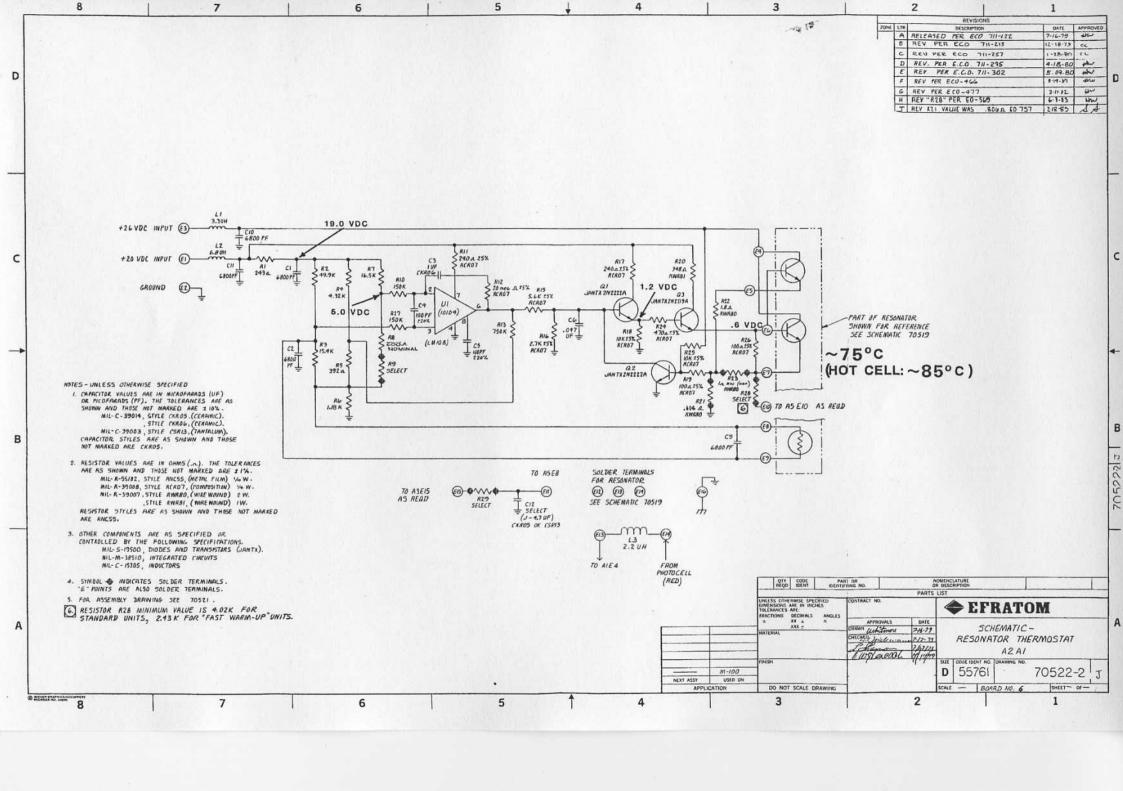
PL 70515-748

CONTRACT NO.

SHEET 4 OF 4

NO.	QTY REQD	FSCM NO.		OR IDENT	DESCR	IPTION				REFE	RENCE
62	1		RJ12FY202	2	POTENT	IOMETER	2ΚΩ		R	35 (7	0515-2
63	4		7041	7-1	STANDO	FF					
64	REF		7051	6	SCHEMA	TIC				250	
65	i								ı		
66	1		RNC55H,332	21FS	RESIST	OR 3.32	ZK NOMINA	L	R	36	
67	1		RNC55H130	1FS	RESIST	OR 1.	30K		R	38	
68	1		RNC55H221	1FS	RESIST	OR 2.	21K		R	39	
69	1		RNC55H845	50FS	RESIST	OR 84	15Ω		R	32	
70	31	200	SE16XC02		TERMIN	AL,SOLDE	R				
71	1		RNC 55 H	2741F\$		THE PERSON NAMED OF THE PARTY OF	2.74 K		R	7 (	0515-2
72	1		RNC55H				4.99 K				515-3
ACT	ONE !		T VIII DOL	. TO AVAI	LABILITY.	SEE ECO	711-200	OK ALTI			
ACT	ONE !	ANT HA	·	. TO AVAI	LABILITY.	SEE ECO	711-200	OK ALTI			
ACT				TO AVAI	LABILITY.	SEE ECO	711-200	OK ALTI			
ACT		ANT HA		TO AVAI	LABILITY.	SEE ECO	711-200	OK ALTI			
ACT		,		. TO AVAI	LABILITY.	SEE ECO	711-200 1	OK ALTI			
ACT		,		TO AVAI	LABILITY.	SEE ECO	711-200	OK ALTI			
ACT		, ,		TO AVAI	LABILITI	SEE ECO	711-200	OK ALT			
ACT		, ,			LABILITI	SEE ECO	711-200	OK ALT			
ACT		,			LABILITI	SEE EUU	711-200	OK ALTI			
ACT		, ,						OK ALTI			
8			RI	EVISION	STATUS O	F THIS	SHEET	OK ALTI			
LET	TER	A 6-20-79	RE	EVISION		F THIS	SHEET	H 5-10-81	J 6-2-83		







FSCM NO.

PL 70521-2

LIST TITLE:

RESONATOR THERMOSTAT ASSY

CONTRACT NO.

SHEET 2 of 3

NO.	QTY REQD	FSCM NO.	PART OR IDENT NUMBER			DESCRIPTION						REFERENCE		
1	1		705	87		PRINTED WIRING BOARD								
2	1		M38510/10104BGX			OP A	OP AMP						U1	
3	2		M39014/0	1-1340		CAPA	CITOR		100PF			C4,C5		
4	5		M39014/0	1-1572		CAPA	CITOR	6	800PF			C1,2,9,10,11		
5			NOT	USED										
6	1		M39014/0	1-1587		CAPA	CITOR		047UF			C6		
7	1		70,5	-129		CAPA	CITOR		1UF			C3		
8	2		JANTX2N2	222A		TRAN	SISTOR					01,02		
9	1		JANTX2N2	219A		TRAN	SISTOR					Q3		
10			NOT	USED										
11	1		RNC55H2430FS			RESI	RESISTOR 243Ω					RI		
12	1		RNC55H3920FS			392Ω						R5		
13	1		RNC55H1181FS			1.18κΩ						R6		
14	1		RNC55H4321FS			4.32ΚΩ						R4		
15	1		RNC55H1542FS			15.4ΚΩ						R3		
16	1		RNC55H1652FS				16.5ΚΩ					R7		
17	1		RNC55H4992FS					49	.9ΚΩ			R2		
18			NOT	USED										
19	1		RNC55H7503FS					7	50ΚΩ			R13		
20	1		RCR07G206JS					20	MEGΩ			R12		
21	2		RCR07G101JS						100Ω			R19,R26		
22	2		RCR07G241JS				240Ω							
23	1		RCR07G471JS						470Ω			R24		
24	1		RCR07G272JS			2.7ΚΩ						R16		
25	1		RCR07G562JS			5.6ΚΩ						R15		
26	2		RCR07G103JS			10ΚΩ						R18,R25		
27	1		RWR8031			.604 Ω 2W						R21		
28	1		RWR81S348			RESISTOR 348Ω 1W						R20		
29			NOT USED				335							
30	1		MS7510.1-1			INDUCTOR 3.3UH (MS75101-1)					1)	L1		
31	1	MS75084-10		INDUCTOR 6.8UH (MS75084-10)						L2				
011				REVISIO	V ST	TATUS	OF T							
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RESONATOR THERMOSTAT ASSY

## PARTS LIST

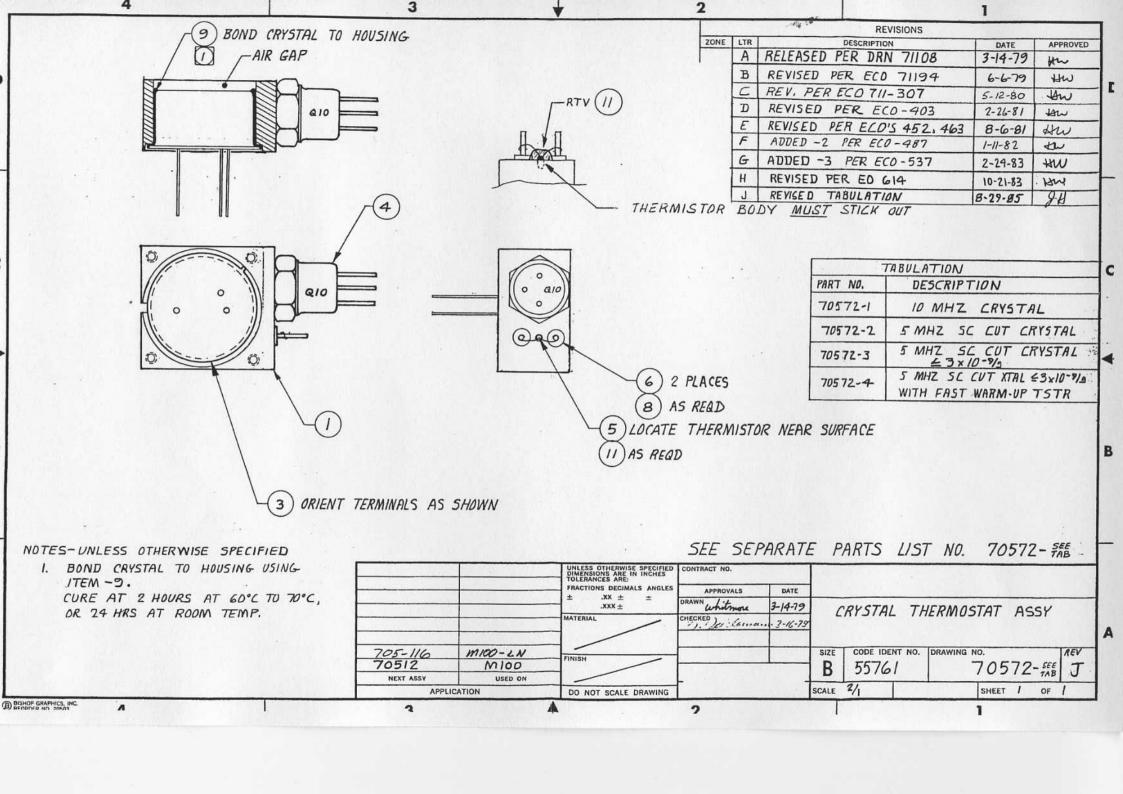
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PL 70521-2

CONTRACT NO.

SHEET 3 OF 3

ITEM		FSCM		OR IDE	NT	DESCRIPTION			<u> </u>			
NO.	REQD	NO.	NUMBER			DECOMPTION .	REFERENCE					
32	1		RNC55H4	021FS		RESISTOR , NOMINAL VALU	R28					
33	1		RNC55H20	000FS		RESISTOR, NOMINAL VALUE	R8					
34	26		704	16-3		TERMINAL, SOLDER						
35	4		704	17-1		STANDOFF, SELF CLINCHING						
36	2		RNC55or	RCRO7_		RESISTOR, SELECT (FS or	JS)	R9, R29				
37	-		NOT	USED		¥						
38	-		NOT	USED								
39	1		704	18-1		MOUNTING PAD		X03				
40	2		M38527/3	-02N		MOUNTING PAD	XQ1,XQ2					
41	1		M38527/4	-03N		MOUNTING PAD		XU1				
42	AR		SN63WRMA	P3		SOLDER						
43	AR		MIL-I-46	058, TY	PE UR	CONFORMAL COAT						
44	2		RNC55H15	03FS		RESISTOR 150K						
45	1		RWR80S1R	82FS		RESISTOR 1.82 A 2W		R10,R27				
46	1					RESISTOR, NOMINAL VALUE, 2W	R23					
47	1		M39014/0	1-1593		CAPACITOR .1UF "SELECT		C12				
48	1		M39003/0	1-2848		CAPACITOR 4.7UF "SELECT	ш ,	C12				
ACTU	AL PA	RT MAY	VARY DUE	TO AVA	ILABI	LITY. SEE ECO 711-260 FOR A	ALTERNATE	VALUES				
			- •		3							
EF	-		TP7052	TP70521 TEST PROCEDURE				4				
EF				SCHEMATIC								
			R	EVISIO	N STA	ATUS OF THIS SHEET						
ETT	ER	A	В	C	D							
DATE		1-28-80	4.18-00	3-11-82	6-3-8.	3						
CO	NO.	111-257	711-267	477	569							





CRYSTAL THERMOSTAT ASSY

LIST TITLE:

DATE

ECO NO.

711-94

6-6-79 7-5-79 9-14-79 11-16-79

711-194

711-235

711-132

## 18851 BARDEEN AVE PARTS LIST

55761

PL 70572-1

6-13-83 11/20/86 6-2-87 9-1-87

1194

1319

1093

564

CONTRACT NO.

SHEET 2 OF 2

NO.	QTY REQD	FSCM NO.	PART OR		DI	ESCRIPT	ION			REFER	ENCE
1	1		70543		НО	USING,	CRYSTAI				
2	- ‡	2	NOT US	ED			COLL.				
3	1		70408			YSTAL					
4	1		70573	-1	TR	ANSIST	OR (	• •		Q10	
5	1		70498	-2			OR, RUG			RT1	
6	2		70276		TE	RMINAL	, HERME	TIC			
7			NOT USE	D .			91112				
8	AR		70424	-15	50	LOTCH	WELD	2216			213.5
9	AR		70424	-4	AD	HESIVE					
10	AR		70411	THE FELL TO	TH	ERMAL	JOINT CO	OMPOUND			
-11			70424	-13	-		- RUBBER			· DOW CORN	ING
								81 (98			
			RE	VISION S	STATU	SOF	THIS S	HEET			

2-26-81

403

8-14-81

463

8-18-81 Hw